Insp Area: 1231 I Street, Sacramento, CA 95814 Sub-Type: **ASFR** Site Address: 256 40TH ST SAC Housing (Y/N): N 0040112008 Parcel No: **ARCHITECT** OWNER **CONTRACTOR** LAINO NICHOLAS J/JAYNEE 256 40TH ST 95819 SACRAMENTO CA Phone: Phone: 916-455-7847 Nature of Work: SECOND STORY ADDITION TO DETACHED GARAGE - STORAGE/EXERCISE - NON-HABITABL CONSTRUCTION LENDING AGENCY: I hereby affirm under penalty of perjury that there is a construction lending agency for the performance of the work for which this permit is issued (Sec. 3097, Civ. C). Lender's Address Lender's Name LICENSED CONTRACTORS DECLARATION: I hereby affirm under penalty of perjury that I am licensed under provisions of Chapter 9 (commencing with section 7000) of Division 3 of the Business and Professions Code and my license is in full force and effect. Contractor Signature License Number Date OWNER-BUILDER DECLARATION: I hereby affirm under penalty of perjury that I am exempt from the contractors License Law for the following reason (Sec. 7031.5, Business and Professions Code; any city or county which requires a permit to construct, alter, improve, demolish, or repair any structure, prior to its issuance, also requires the applicant for such permit to file a signed statement that he or she is licensed pursuant to the provisions of the Contractors License Law (Chapter 9 (commencing with Section 7000) of Division 8 of the Business and Professions Code) or that he or she is exempt therefrom and the basis for the alleged exemption. Any violation of Section 7031.5 by any applicant for a permit subjects the applicant to a civil penalty of not more than five hundred dollars (\$500.00); I, as a owner of the property, or my employees with wages as their sole compensation, will do the work, and the structure is not intended or offered for sale (Sec. 7044, Business and Professional Code: The Contractors Law does not apply to an owner of property who builds or imporves thereon, and who does such work himself or herself or through his or her own employees, provided that such improvements are not intended or offered for sale. If, however, the building or improvement is sold within one year of completion, the owner-builder will have the burden of proving that he or she did not build or improve for the purpose of sale.) I, as owner of the property, am exclusively contracting with licensed contractors to construct the project (Sec. 7044, Business and Professions Code: The contractors License Law does not apply to an owner of property who builds or improves thereon, and who contracts for such projects with a contractor(s) licensed pursuant to the Contractors License Law). I am exempt under Sec B & PC for this reason: Owner Signature IN ISSUING THIS BUILDING PERMIT, the applicant represents, and the city relies on the representation of the applicant, that the applicant verified all measurements and locations shown on the application or accompanying drawings and that the improvement to be constructed does not violate any law or private agreement relating to permissible or prohibited locations for such improvements. This building permit does not adhorize any illegal location of any improvement or the violation of any private agreement relating to location of improvements. Applicant/Agent Signature WORKER'S COMPENSATION DECLARATION: 1 hereby affirm under penalty of perjury one of the following declarations: I have and will maintain a certificate of consent to self-insure for workers' compensation as provided for by Section 3700 of the Labor Code, for the performance of work for which the permit is issued. I have and will maintain workers' compensation insurance, as required by Section 3700 of the Labor Code, for the performance of the work for which this permit is issued. My workers' compensation insurance carrier and policy number are:

CITY OF SACRAMENTO

Carrier

Permit No: 9712626

WARNING: FAILURE TO SECURE WORKER'S COMPENSATION COVERAGE IS UNLAWFUL AND SHALL SUBJECT AN EMPLOYER TO CRIMINAL PENALTIES AND CIVIL FINES UP TO ONE HUNDRED THOUSAND DOLLARS (\$100,000) IN ADDITION TO THE COST OF COMPENSATION, DAMAGES AS PROVIDED FOR IN SECTION 3706 OF THE LABOR CODE, INTEREST AND ATTORNEY'S FEE.

subject to the workers' compensation provisions of Section 3700 of the Labor Code shall proposition states of the section 3700 of the Labor Code shall proposition to the workers' compensation provisions.

Applicant Signature

(This section need not be completed if the permit is for \$100 or less) I certify that in the performance of the work for which this permit is issued, I shall not employ any person in any manner so as to become subject to the workers' compensation laws of California and agree that if I should become

Policy Number

2987 X

CITY OF SACRAMENTO DEVELOPMENT SERVICES DIVISION

EXPRESS PLAN REVIEW

		DAT	ES		
1ST R	EVIEW	RECH	ECK	2ND RE	CHECK
IN / (C)	9 OUT	IN 91/2/57	OUT	IN / /	OUT /
	Bun	, ,		<u> </u>	

am

PLAN CHECK NO. 52906 2787	COMM.	RES.
CONTACT PERSON: Nick LAINO	PHONE: 916-	455-7847
PROJECT ADDRESS: 256 40TH STREET SAC. 95819	FAX: 916-4	155-7837
DESCRIPTION OF WORK: 5900ND STORY ADDITION to		

	1s	1st Review			RECHECK			2ND RECHECK		
DISCIPLINE	EPR	ос	APPR	EPR	OC	APPR	EPR	oc	APPR	
LIFE SAFETY			1DC							
STRUCTURAL	12.77 1.12.1	+,				9-19-	7			
MECHANICAL/PLUMBING			WA			******		1	,	
ELECTRICAL		(/	MAN	TC	W	u				
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PLANNING		1	•	SIAA	L 5	TAM	bf	519	2	
			- Carrier Marie	DR	MAG		47			

Legend:

EPR = OK for Express Plan Review
OC = OK for Over the Counter Recheck
APPR = Approved as submitted

9/12/97 fored commont our

COMMERCIAL PLAN CHECKING/PERMIT SERVICES SECTION

PO 1 99 11/2	ADDRESS 2	510	Hom	_55	
am in receipt of the abo completion with the appro failure in returning the plan permit and may constitute	priate corrections. ns to the Building	. I am awa Departmer	are of the fact nt may delay	that my delay o	r
NOTE: RETURN CHECK S and date all revisions with n column where correction w	next submittal of pla	ans, indicate			
REPRESENTATIVE		COMPA	NY REPRESE	NTING	
DATE					
	CITY USE	ONLY			_
NOTE ON COMPUTER:					<u>-</u>
TATE OUT: 9 25	DATE	RETURNED	:		<u>.</u>
# OF BLDG SETS:	# OF	BLDG SETS	RET:		
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# OF CYCLES:	# OF	CYCLES RE	т:		
CHECKED OUT BY:	RETU	JRNED TO:			
DATA ENTRY (OUT) BY:	DATA	LENTRY (RE	n) BY:		



DEPARTMENT OF PLANNING AND DEVELOPMENT

Sacramente Cal 95814

Administration
Room 300 449-5511
Building Inspections
Room 200 449-5116
Planning
Room 200 449-5664

Dear Plan check applicant:

It is our aim to provide accurate and efficient plan checking service to you. In order to make this possible, we request that when submitting revisions you adhere to the following guidelines:

- Submit all revisions with a transmittal letter that lists the page number of the sheets being revised. State the disciplines being affected, and if possible enclose a copy of the city plan checker's correction list.
- Please cloud, delta and date all revisions; (yellow lined acceptable).
- 3. It is essential that all plan check revisions be marked with the plan check number and complete address when submitted or messengered in. We will only accept plans which provide this information.
- 4. Make sure that the re-submittal package is complete; that **all** disciplines requiring revisions are submitted at the same time.
- 5. You must submit the **same** number of plans for **revisions** that you did for **the original plan check**. (Generally, four sets for shells, buildings, additions and site work; two for all others).
- 6. Revised sheets with Title 24 energy information must be stamped by the original T-24 review consultant prior to permit issuance.
- 7. If possible, have the plan checker briefly review the revisions at the counter to ensure compliance with information requested.

It is our hope that the above suggestions will expedite the plan re-check process for everybody. Please let us know if you have any additional suggestions on how we may better accommodate your needs.

Date 9/1+/577

REUISIONS

THIS SHEET IS TO BE USED WHEN PLANS ARE SUBMITTED WITH PLAN CHECK CORRECTIONS OR REVISIONS ON A PLAN WHICH IS STILL IN THE PLAN CHECK PROCESS.

ORIGINAL ROUTE	В	L	Р	М	E	F	S	D	R
Status (opt)									
	В	L	P	М	E	F	S	D	R
Revision to be routed to (order)	13	}							
and sets submitted	i	<u> </u>	BY PHO	(NAME	:>	App	450	k G	4/NO 342
Dlan Address				40	+2	14			

Plan Address _	156,0	40 te	Hu	
Plan Check #	2087			
Submitted to				
			-	

KEEP TRACK OF HOURS? YES No

COMMERCIAL PLAN CHECKING/PERMIT SERVICES SECTION

PC 3787 ADDRESS 356-40 57

completion with the appropriate corre	and I will return the plans upon my review and ections. I am aware of the fact that my delay or Building Department may delay the issuance of a erecheck of the plans.
	ANS WITH NEXT SUBMITTAL! Please cloud, delta, tal of plans, indicate detail and sheet number in last on plans.
REPRESENTATIVE	
REPRESENTATIVE	COMPANY REPRESENTING
7 15 97	
DATE	
	CITY USE ONLY
	CITY USE ONLY
NOTE ON COMPUTER:	
DATE OUT: 975 77	DATE RETURNED:
# OF BLDG SETS:	# OF BLDG SETS RET:
# OF SITE SETS:	# OF SITE SETS RET:
# OF CYCLES:	# OF CYCLES RET:
CHECKED OUT BY:	RETURNED TO:
DATA ENTRY (OUT) BY:	DATA ENTRY (RET) BY:



DEPARTMENT OF PLANNING AND DEVELOPMENT

Sacrament: Cal 95814

Administration
Room 300 449-5511
Building Inspections
Room 200 449-5116
Planning
Room 200 449-5604

Dear Plan check applicant:

It is our aim to provide accurate and efficient plan checking service to you. In order to make this possible, we request that when submitting revisions you adhere to the following guidelines:

- 1. Submit all revisions with a transmittal letter that lists the page number of the sheets being revised. State the disciplines being affected, and if possible enclose a copy of the city plan checker's correction list.
- Please cloud, delta and date all revisions; (yellow lined acceptable).
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- 4. Make sure that the re-submittal package is complete; that **all** disciplines requiring revisions are submitted at the same time.
- 5. You must submit the same number of plans for revisions that you did for the original plan check. (Generally, four sets for shells, buildings, additions and site work; two for all others).
- 6. Revised sheets with Title 24 energy information must be stamped by the original T-24 review consultant prior to permit issuance.
- 7. If possible, have the plan checker briefly review the revisions at the counter to ensure compliance with information requested.

It is our hope that the above suggestions will expedite the plan re-check process for everybody. Please let us know if you have any additional suggestions on how we may better accommodate your needs.

FLOOR FRAMING

BCI Joists

NOTE

The Justration below is showing several suggested applications for the Boise Cascade products.

It is not intended to show an actual house under construction

PC 2987 x BCI joist blocking or 2x4 "squash" block on each side required when supporting a load-bearing wall above.

or a BCI joist header.

HOISIAN HORING INDIAMEZORS VERSA-LAM header

NOT DEPAY BRIDGING FOR INSTALLATION STABILITY. Temporary strut lines (1x4 min.) 8' on center max Faster at each joist with 2-8d nails min.

11/2" knockout holes at approximately 12" o.c. are pre-punched.

> See page 12 for allowable hole sizes and location

80 million

where hearing length allows) will supply 12000 bs per lineal

toot on sectional loak

VERSA RIM 98 nm board will support 4000 as per lineal toot of vertical load

hacabac bearing cantilever details, see page 13

Lateral support managed when BCI joists are cantilevered. Use BCI joist blocking for at seas Decigies pay, 25 feet of bearing wall length and at least 4 feet on each end of antilevered are

Endwall blosting may be required.

ЭC		of Marie		45	SERIES - 13	4" FLANGE W	/IDTH		60 SERIES	- 25/16" FLA	NGE WIDTH	
spacing	797			91/2"	11%"	14"	16"	117/8"	14"	16"	18"	20"
					* CO	DE APPRO	OVED ★				<u></u>	
	- 1° - 1' _	21 - 7'	24 - 6	19 - 2"	22 - 10"	25' - 11"	28' - 9"	24' - 8"	28' - 0"	30' - 0"	30' - 0"	30' - 0"
· 5.	. 'n 6 <u>"</u>	19 - 6"	21 - 8"	17 - 5"	20 - 9"	23' - 7"	26' - 2"	22' - 5"	25' - 5"	28' - 2"	30' - 0"	30' - 0"
# <u>2</u>	16 5"	17 - 10'	19 - 9"	16 - 5"	19 - 7"	21 - 10"	24' - 5'	19" - 10"	21' - 10"	24' - 11"	29' - 0"	30 - 0"
. ~	47 9.	15 10	17 5"	13 - 9"	15 - 10"	17' - 5"	19' - 11"	15' - 10"	17' - 5"	19' - 11"	24' - 8"	27' - 10'
No	4"	1 10	13 1	10 4	11 - 10	13' - 1'	14' - 11"	11' - 10"	13' - 1"	14' - 11"	18' - 5"	20' - 10"
					***1	HREE STA	R ★★★					
12	16 4"	19' - 5"	22 - 1"	17' - 3"	20' - 7"	23 - 5"	25' - 11"	22' - 3"	25' - 3"	28' - 0"	30' - 0"	30" - 0"
1 €	14 10"	17 - 8"	20' - 1"	15" - 8"	18 - 8"	21' - 3"	23' - 6"	20' - 2"	22' - 11"	25' - 4"	27' - 9"	30' - 0"
9.2	1.1 0"	16 - 8"	18' - 11"	14 - 9"	17' - 7"	19' - 11"	22' - 1"	18' - 11"	21' - 6"	23' - 10"	26' - 1"	28' - 3"
24	<u> 12 11'</u>	15' - 5"	17" - 5"	13' - 8"	15' - 10"	17' - 5"	19' - 11"	15' - 10"	17' - 5"	19' - 11"	24' - 1"	26' - 1"
32	10 4"	11 - 10"	13 - 1"	10' - 4"	11' - 10"	13 - 1"	14' - 11"	11' - 10"	13' - 1"	14' - 11"	18' - 5"	20' - 10"
					****	OUR STAI	R ****					
. 12	6"	15' - 0"	17' - 1'	11 - 6"	15' - 11"	18' - 1"	20' - 1"	17' - 2"	19' - 6"	21' - 7"	23' - 8"	25' - 8'
16	1 5	13' - 7"	15' - 6"	11 - 6"	14' - 4"	16' - 4"	18' - 1"	15' - 5"	17' - 7"	19' - 6"	21' - 4"	23 - 1"
19.2	H 0.7	12 - 9"	14 - 6"	10 - 0"	13' - 5"	15 - 3"	16' - 11"	14' - 5"	16' - 5"	18' - 2"	19' - 11"	21' - 7"
2.4	3 0.	11 . 9"	13' - 4"	10 - 0"	12 - 4"	14' - 1"	15' - 7"	13' - 3"	15' - 1"	16' - 9"	18' - 4"	19' - 11"
32	8	10 4	11 10"	8' 7"	10 - 4"	11' - 10"	13' - 2"	11' - 2"	12' - 9"	14' - 2"	15' - 7"	16' - 11"

Span tables assume that sheathing is glued and nailed to joists.

Spans represent the most restrictive of simple or multiple span applications.

Span tables are based on a residential floor load of 40 PSF live load and 10 PSF dead load, and a clear distance between supports.

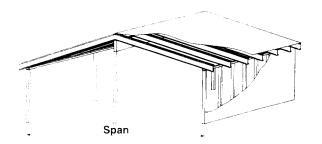
- Code allowed live load deflection at L'360, see page 3 "about floor performance guide" for additional data.

*** Live Load deflection at L/480.

★★★★ Eive Linad deflection at Li960 to give a floor that is much stiffer for the more discriminating purchaser.

ROOF RIDGE BEAMS

Versa-Lam Beams



noisivid anibliad

OOF OADING	COLUMN SPACING	SPAN O	SUPPORTED	ROOF FRAMI	NG (SUM OF S	PANS ON BOT	H SIDES OF B	EAM IN FT.)
	(FT.)	20	24	26	30	32	36	40
Non-Snow	14'	31/- x 91/2	31/2 x 117%	31/2 x 117/8	31/2 x 117/8	3 ¹ / ₂ x 11 ⁷ / ₈	31/2 x 14	3½ x 14
125%)			51/4 x 91/1	51/4 x 91/2	51/4 x 91/2		374 x 11 1/8	5!/4 x 117/
0 PSF Live	18'	31/ x 14	31/2 x 14	31/a x 14	31/2 x 16	31/2 x 16	31/2 x 16	3½ x 16
		51/4 x 117/8	51/4 x 11/8	5¼ x 117/a	$5^{1/4} \times 14$	51/4 x 14	51/4 x 14	5½ x 14
PSF Dead	22'	31/2 x 16	31/2 x 16	3½ x 18	31/2 x 18	31/2 x 18		
		51/4 x 14	5½ x 14	51/4 x 16	51/4 x 16	51/4 x 16	51/4 x 16	51/4 x 16
on-Snow	14'	31/: x 117/a	31/2 x 117-6	3½ x 14	31/2 x 14	31/2 x 14		
125%)		51/4 x 91/2		51/4 x 117/8	51/4 x 117/8	5 ¹ / ₄ x 11 ⁷ / ₈	5 ¹ / ₄ x 11 ⁷ / ₈	5½ x 14
PSF Live	18'	3½ x 14	3½ x 16					
		51/4 x 117/8	51/4 x 14	51/4 x 14	51/4 x 14	51/4 x 16	51/4 x 16	51/4 x 16
PSF Sead	22	3¹/₂ x 18						
		574 x 16	5½ x 16	51/4 x 16	51/4 x 16	51/4 x 18	51/4 x 18	
now	14'	31/2 x 91/2	31/2 x 91/3	31/2 x 91/5	31/2 x 91/2	31/2 x 117/8	31/2 x 117/8	31/2 x 117/
115%)		51/4 x 71/4				51/4 x 91/2	5 ¹ / ₄ x 9 ¹ / ₂	5½ x 9½
PSF LIVE	18'	31// _x x 117/ ₈	31/2 x 117/-	31/2 x 117/8	31/2 x 14	31/2 x 14	31/2 x 14	31/2 x 14
		51/4 x 91/2			51/4 x 117/8	51/4 x 117/8	5¹/4 x 11²/8	51/4 x 117/
PSF Dead	22	3½ x 14	3°/2 x 14	31/2 x 16	31/2 x 16	31/2 x 16	31/2 x 18	31/2 x 18
		51/4 x 117/8		51/4 x 14	51/4 x 14	51/4 x 14	51/4 x 14	51/4 x 16
now	14	31/:: x 91/2	3½ x 9%	31/2 x 91/3	31/2 x 117/8	31/2 x 117/8	31/2 x 117/8	31/2 x 117/8
15%)					51/4 x 91/2	5 ¹ / ₄ x 9 ¹ / ₂	51/4 x 91/2	51/4 x 91/2
PSF Live	18'	31/: x 117/8	31/2 x 117	3½ x 14	31/2 x 14	31/2 x 14	3½ x 16	3½ x 16
				51/4 x 117/8	5 1/4 x 117/8	5 ¹ / ₄ x 11 ⁷ / ₈	5 ¹ / ₄ x 11 ⁷ / ₈	5 ¹ / ₄ x 1 4
PSF Dead	22	316 x 14	31/2 x 16	31/2 x 16	31/2 x 16	3½ x 18	31/2 x 18	5 ¹ / ₄ x 16
		51/4 x 117/8	51/4 x 14	51/4 x 14	51/4 x 14	5 ¹ / ₄ x 14	51/4 x 16	0 74 X 10
now	14	3 /2 x 91/2	31/2 x 117/4	3½ x 11½	3¹/2 x 11²/8	31/2 x 117/8	31/2 x 14	31/2 x 14
15°₀)			51/4 x 91/2	51/4 x 91/2	51/4 x 91/2	0 12 X 11 18	5 ¹ / ₄ x 11 ⁷ / ₈	5 ¹ / ₄ x 11 ⁷ / ₈
PSF Live	18	31/2 x 14	3½ x 14	31/c x 14	3 /2 x 16	3¹/2 x 16	5 ¹ / ₄ x 14	$\frac{5.74 \times 11.78}{51/4 \times 14}$
PSF Dead		51/4 x 117/8	51/4 x 14	51/4 x 14	51/4 x 14	51/4 x 14	3 /4 X 14	374 X 14
rsr Dead	22	31-2 x 16	3½ x 16	3¹/₂ x 18	5¹/4 x 16	5 ¹ / ₄ x 16	51/4 x 16	5 ¹ / ₄ x 18
		5¼ x 14	51/4 x 14	5⅓ x 16		0 /4 X 10	3 /4 X 10	J /4 X 10
now	14'	31/2 x 117/8	31/2 x 117/F	31/2 x 117/8	3'/2 x 14	31/2 x 14	31/2 x 14	5 ¹ / ₄ x 11 ⁷ / ₈
15%)	:	51/4 x 91/2	51/4 x 91/2		51/4 x 117/8	5 ¹ / ₄ x 11 ⁷ / ₈	5 ¹ / ₄ x 11 ⁷ / ₈	J /4 X 111/8
PSF Live	18	31/a x 14	3'/2 x 16	3½ x 16	51/4 x 14	5 ¹ / ₄ x 14	5 ¹ / ₄ x 16	5 ¹ / ₄ x 16
		51/4 x 117/8	51/4 x 14	51/4 x 14		J	J /4 A 10	J /4 X 10
PSF Dead	22	31/2 x 18	3½ x 18	5' x 16	5½ x 18	5½ x 18	5 ¹ / ₄ x 18	
		514 x 14	51/4 x 16		5 n 10	0 /4 X 10	5 /4 X 10	

NOTES

- Deflection is limited to L/240 at live load and to L/180 at total load.
- Assumes bearing length of 3" at each end and 4½" in shaded area.
- Also assumes a bearing length of $7^{1}\!/\!\epsilon^{\prime\prime}$ at intermediate support and 101% in shaded area
- Values based on most restrictive of simple or continuous beam span
- Sizes shown are for one-piece applications. For multiple members of 1 9/4" Versa-Lam please contact your distributor or dealer for additional information.

Muiti-Loaded Beam(94 UBC (91 NDS) | Ver. v4031216 ov: HOWARD G. TAYLOR , HGT Architect on: 09-16-1997

Fefections	3.50 IN x 16.00 IN x 19.6 FT / 2.0E WS Parallam - TRUS JOIST-MACMILL Section Adequate By: 18.9% Controlling Factor: Section Modulus / Depth	.AN Required 14.77	7 In	
LUD) N 1
TIDE 0.77 IN = D TIDE 0.77 IN IN TIDE 0.77 IN IN TIDE D TIDE 0.77 IN IN TIDE 0.77 IN IN TIDE D TIDE 0.77 IN IN TIDE 0.77 IN IN TIDE D TIDE 0.77 IN IN TIDE 0.77 IN IN TIDE D TIDE 0.77 IN IN TIDE 0.77 IN IN TIDE D TIDE 0.77 IN IN TIDE 0.77 IN IN	⊃ead Load:			
Proceedings	Live Load:			
Live Load Rt	Total Load:	TLD=	0.77	N = □
Let Load Rt	End Reactions(Left Side):			
Dead Load RD1= 4572 LB		RL1=		
Total Load Total Readtins (Right Side) Live Load Dead Load: Potal Load: Potal Load: Bearing Length Read.(Left) Bearing Length Read.(Right) Peam Data Span Maximum Inbraced Span: Live Load Deflect Criteria: Live Load Load: Live Load Load: Live Load Load: Live Load Load: Live		RD1=	2221	LB
Beautions(Right Side)		RT1=	4572	LB
Dead Load Dead Load RD2= 2245 LB				
Dead Load:		RL2=	2384	LB
State Coad State		PD2=		
Bearing Length Repd (Right) BL2	Total Load:	RT2=		
Bearing Length Repd (Right) BL2	Seering Length Road / Loft)	194181118111=		
### Data		B) 2=		
Span	4.1 mg		2.00	11 4
Dead Defined Circle Dead Defined Circle Dead Load	Beam Data.	1	10.6	CT
Dead Defect. Criteria Dead Defect. Criteria Dead Dead Dead Dead Load	Span:	Q		
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Dead Defect. Criteria Dead Defect. Criteria Dead Dead Dead Dead Load	Sive Load Duration Factor:	∵α =		
Dead Defined: Criteria Dead Defined: Criteria Dead Dead Dead Dead Dead Dead Dead Dead	Live Load Deflect. Criteria:	<u> </u>		
Live Load	otal Load Deflect. Criteria:		240	
Dead Load: BSW	োniform Load:			
Heam Self Weight:	Live Load.			
Total Load: Indicators WT= 327 PLF Indicators PL1= 1600 LB Indicators PD1= 1200 LB Indicators PT1= 2800 PSI Indicators PT2 PSI Indicators PT3 PL5 PSI Indicators PT4 PSI Indicators PT4 PSI Indicators PSI PSI PSI Indicators PSI PSI PSI Indicators PSI PSI PSI PSI Indicators PSI PSI	⊝ead Load:		153	
Total Load: Incentrated Load P1: Live Load Dead Load: Dead Load: Dead Load: Total Load: Dead Load:		BSW=	14	PLF
PL1	5	wT=	327	PLF
PL1= 1600				
Dead Load:		PL1=	1600	LB
otal Load:				
Name				
Properties For: 2.0E WS Parallam- TRUS JOIST-MACMILLAN Bending Stress: Fv= 290 PSI				
Bending Stress: Fb= 2900 PSI		, , , ,	10.0	
Shear Stress		Fh=	2900	PSI
Modulus of Elasticity: Stress Perpendicular to Grain: Fc_perp= 650 PSI				
Stress Perpendicular to Grain: Fc_perp 650 PSI				
Adjusted Properties: - b (Tension):		_		
## Adjustment Factors: Cd=1 00 Cf=0.97 Adjustment Factors: Cd=1 00 ### Esign Requirements: Maximum Moment:		rc_perp-	030	F 31
Adjustment Factors: Cd=1 00 Cf=0.97 Adjustment Factors: Cd=1 00 esign Requirements:		Fh.I	2000	DCI
Adjustment Factors: Cd=1 00 esign Requirements		⊢ υ –	2009	P31
Adjustment Factors: Cd=1 00 lesign Requirements:			200	201
Maximum Moment:	• •	⊢ ∨ ′=	290	PSI
Maximum Moment:				
Maximum Moment:	esign Requirements:			
10.002 FT From Left Support Shear (@ d from beam end) Smparisons With Required Sections: Section Modulus: Sreq= 125.6 IN3 S= 149.3 IN3 Area: Area: Area= 21.7 IN2 A= 56.0 IN2 Ireq= 940.4 IN4 I= 1194.6 IN4		M=	29389	FT-LB
Shear (@ d from beam end) Smparisons With Required Sections: Section Modulus: Sreq= 125.6 IN3 S= 149.3 IN3 Area Areq= 21.7 IN2 A= 56.0 IN2 Ireq= 940.4 IN4 I= 1194.6 IN4				
Section Modulus: Sreq = 125.6 IN3 IN3 IN3 IN3 IN4		V=	4194	LB
Section Modulus: Sreq= 125.6 IN3 S= 149.3 IN3 Areq= 21.7 IN2 A= 56.0 IN2 Ireq= 940.4 IN4 I= 1194.6 IN4				
S= 149.3 IN3 Area: 21.7 IN2 A= 56.0 IN2 Ireq= 940.4 IN4 I= 1194.6 IN4		Sreq=	125.6	IN3
Area: Area	7001011 1/13 do 1401			IN3
Moment of Inertia: A= 56.0 IN2 Ireq= 940.4 IN4 1194.6 IN4	area:	Area=		IN2
Vioment of Inertia:	1			
1194.6 IN4	Moment of Inertia:			
mul m	Violities of method			
July and July 2009		,		
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Roof Beamf 94 UBC (91 NDS)] Ver. v4031216 By: HOWARD G. TAYLOR: HGT Architect on: 09-16-1997

By: HOWARD G. TAYLOF	R HGT Architect on: 09-16-1997		
Project BOLDEN - Location: lateral ridge beams Summary			
3 50 IN x 7.25 IN x 10.0 FT / Select Structural - DOUGLAS Section Adequate By: 28.0% Controlling Factor: Section N	S FIR-LARCH (NORTH) - Dry Usi Modulus / Depth Required 6.41 In	9	
Deflections	DLD=	0.16	IN
⊃ead Load:	LLD=	0.10	IN = L/704
Live Load: Total Load:	TLD=	0.33	IN = ∐/363
Reactions (Each End):	, 22	5.55	
_ive Load:	RL=	800	LB
Dead Load:	RD=	752	LB
Total Load:	RT=	1552	LB
Bearing Length Reqd.:	BL=	0.71	IN
Beam Data	1 -	10.0	FT
Span	L= Lu=	10.0 0.0	FŤ
Maximum Unbraced Span:	`````	8.00	12
Pitch Of Roof: Live Load Deflect, Criteria:	RP= U U ownerd ownerdy	240	. (2
Total Load Deflect, Criteria:	The Great and The Control of the Con	180	
Beam Loading			
Live Load	+24 m	16	PSF
Roof Loaded Area:	RLA=	100	SF
Roof Live Load Method: 1			
Side One: Roof Dead Load:	DL1=	12	PSF
Roof Rafter Tributary Width:	TW1=	5.0	FT
Side Two: Roof Dead Load:	TW2=	12 5.0	PSF FT
Roof Rafter Tributary Width:	Cd=	1.15	ΓΊ
Root Duration Factor: Slope Adjusted Lengths and Loads:	Ou-	1.10	
Adjusted Beam Length:	Ladi=	10.0	FT
Beam Live Load W/ Slope Red'n	wL=	160	PLF
Beam Self Weight:	BSW=	6	PLF
Beam Total Dead Load:	wD=	150	PLF
Total Maximum Load:	wT=	310	PLF
Controlling Total Design Load:	wTcont=	310	PLF
Properties For: Select Structural- DOUGLAS FIR-LARCH (NORTH)	Ch-	1200	nei
Bending Stress:	Fb= Fv=	1300 95	PSI PSI
Shear Stress:	E=	1900000	PSI
Modulus of Elasticity: Stress Perpendicular to Grain:	Fc perp=	625	PSI
Adjusted Properties.	, o_perp	020	, 3.
Fb Tension).	Fb'=	1943	PSI
Adjustment Factors: Cd=1 15 Cf=1 30			
÷v	Fv'=	109	PSI
Adjustment Factors: Cd=1 15			
Design Requirements.	14-	2000	CT (O
Maximum Moment:	M= V=	38 80 1 364	FT-LB LB
Shear (@ d from beam end):	V	1304	LD
Comparisons With Required Sections: Section Modulus:	Sreg=	24.0	IN3
Section Modulus.	S=	30.6	N3
irea	Areq=	18.8	IN2
	A=	25.3	IN2
Moment of Inertia:	req=	55.2	iN4
	;* ∖ , <u> </u> =	111.1	IN4
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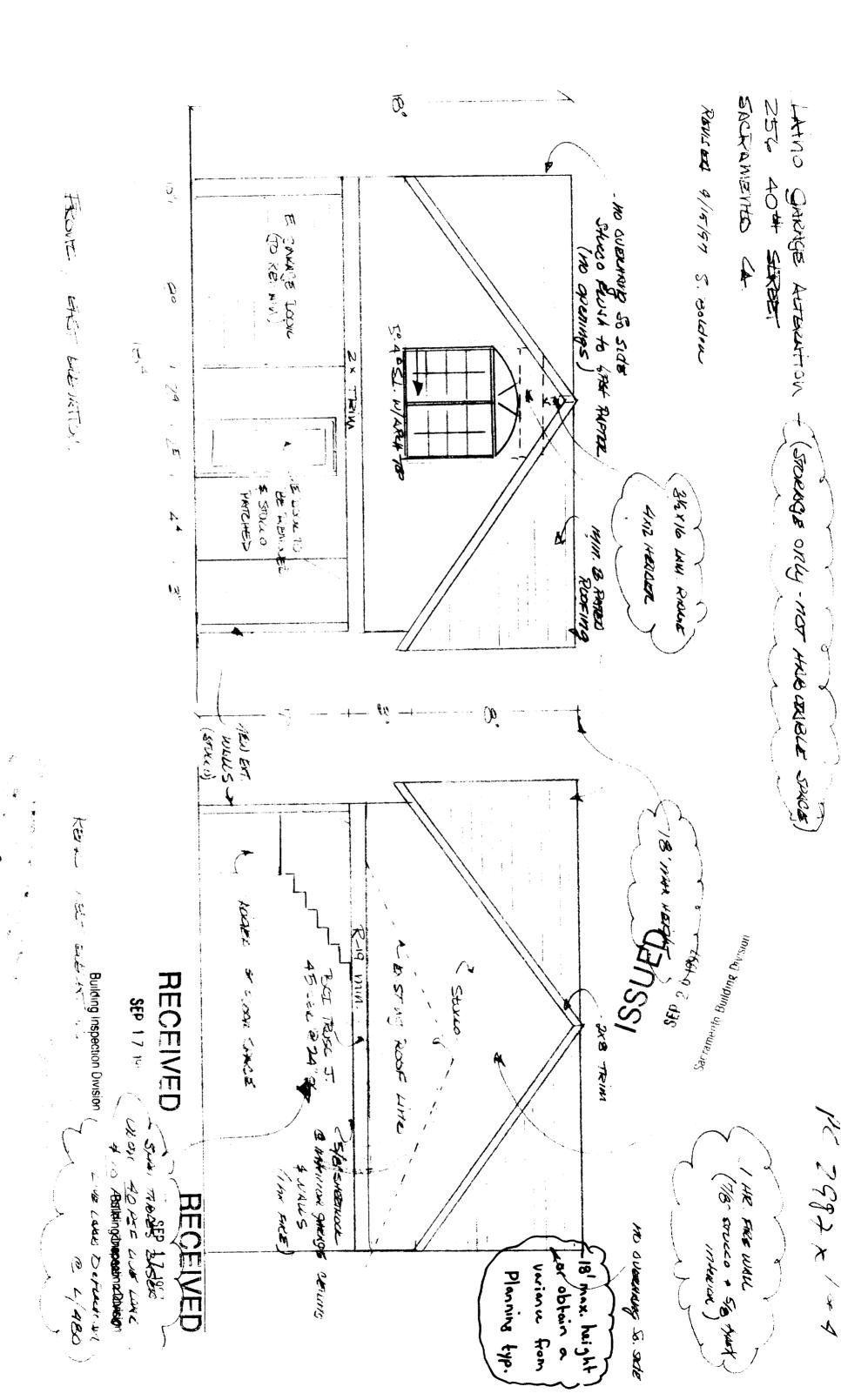
Roof Beam[94 UBC (91 NDS)] Ver. v4031216 By: HOWARD G. TAYLOR , HGT Architect on: 09-16-1997

By: HOWARD G. TAYLOR , HGT Archite	ect on: 09-16-1997		
Project BOLDEN - Location: valley			
Summary			
1.75 IN x 11.875 IN x 12.0 FT (Actual 14.422 FT) / 1.8E WS MicroLam -	TRUS JOIST-MAC	MILLAN	
Section Adequate By: 53.4% Controlling Factor: Section Modulus / Dept	h Required 9 97 In		
Deflections			
Dead Load:	DLD=	0.28	IN
	LLD=	0.29	IN = L/488
Live Load:	TLD=	0.57	1N = L/253
Total Load:	160-	0.57	111 - 0255
Reactions (Each End):	RL≖	960	LB
Live Load:			-
Dead Load	RD=	896	LB
Total Load:	RT=	1856	LB
Bearing Length Reqd.	BL=	1.41	IN
Beam Data	Bur		
Span.	State Sale	12.0	FT
Maximum Unbraced Span:	V &y	0.0	FT
Beam End Elevation Diff.	EL#///	8.0	FT
Pitch Of Roof:	RP= °₹	8.00	: 12
ive Load Deflect. Criteria:	$\mathcal{A}{\mathcal{A}}$ U	¹⁶⁰ 240	
Total Load Deflect. Criteria:	\sim \sim \sim	180	
Beam Loading.	الكنع محا		
Live Load:	"> LĽ=7322	16	PSF
Roof Loaded Area:	RLA=	120	SF
Roof Live Load Method: 1			•
Side One. Roof Dead Load	/O(1=	12	PSF
Roof Rafter Tributary Width:	TWn±	5.0	FT
Side Two: Roof Dead Load:	ni ⊅±	12	PSF
Roof Rafter Tributary Width:	TW2=	5.0	FT
Roof Duration Factor:	Cd=	1.15	1 1
	Cu-	1.13	
Slope Adjusted Lengths and Loads:	l adi-	14 400	C- T
Adjusted Beam Length:	Ladi=	14.422	FT
Beam Live Load W/ Slope Red'n	WL=	133	PLF
Beam Self Weight:	BSW=	4	PLF
Beam Total Dead Load:	w <u>D</u> =	124	PLF
Total Maximum Load:	_ wT=	257	PLF
Controlling Total Design Load:	wTcont=	257	PLF
Properties For: 1 8E WS MicroLam- TRUS JOIST-MACMILLAN			
Bending Stress:	Fb=	2600	PSI
Shear Stress:	Fv=	2 85	PSI
Modulus of Elasticity:	E=	1800000	PSI
Stress Perpendicular to Grain	Fc_perp=	750	PSI
Adjusted Properties:	,		
Fb (Tension):	Fb'=	2 994	PSI
Adjustment Factors: Cd=1.15 Cf=1.00			
ε _υ	Fv'=	3 28	PSI
Adjustment Factors: Cd=1 15	• •		
Design Requirements:			
Maximum Moment:	M=	6 691	FT-LB
Shear (@ d from beam end):	V=	1601	LB
Companisons With Required Sections:	•	1001	
Section Modulus:	Srea=	26.9	IN3
Section Middalas.	S= S=	41.1	IN3
Area	Areq=	7.4	IN2
ਜ਼ਰੂਰ	Areq= A=	20.7	IN2 IN2
Moment of Inortia	rea=	20.7 1 44 .8	N4
Moment of Inertia.			IN4 IN4
	!-	244.2	1114

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Multi-Loaded Beam[94 UBC (91 NDS)] Ver. v4031216 By: HOWARD G. TAYLOR: HGT Architect on: 09-16-1997

By: HOWARD G. TAYLOR , HGT			
Project BCLDEN - Location: header	Architect on: 00-10-10	07	
Surnmary			
3 50 IN x 11.25 IN x 5.0 FT / Select Structural - DOUGLAS FIR-LA	ARCH (NORTH) - Dry U	Jse	
Section Adequate By: 3.0% Controlling Factor: Area / Depth Requirements	urea 10.93 in		
Dead Load	DLD=	0.01	IN
Live Load:	LLD=	0.01	IN = L/4422
Total Load:	TLD=	0.03	IN = L/2263
End Reactions(Left Side).		4444	. 5
Live Load:	RL1= RD1=	1144	LB
Dead Load: Total Load:	RT1=	1102 2246	LB LB
End Reactions(Right Side):	13.1.1	2240	
_ive Load(RL2=	1240	LB
Dead Load:	RD2=	1191	LB
Total Load:	RT2=	2431	LB
Bearing Length Read (Bight)	BL1=	1.03 1.11	IN IN
Bearing Length Reqd.(Right): Beam ⊜ata		7.11	114
Span	BL2= ³ / _{0/3} L= ³ / _{0/4} u= Cor r	5.0	FT
Maximum Unbraced Span:	°€/Ju=	0.0	FT
Live Load Duration Factor:	7%	1.00	
Live Load Deflect. Criteria:	5	360 240	
Total Load Deflect, Criteria: Brilform Load:	107 O . U	S _{SS} 240	
يناورد عامل المعالم الم المعالم المعالم	inns of €wL=	· 6- 0	PLF
Dead Load:	ું ે બંજી ∻ ા	Ō	PLF
Beam Self Weight:	BSW	10	PLF
Total Load:	<i>" ,</i> wT=	10	PLF
Tencentrated Load P1	[†] े ि 1∉−	2384	LB
Live Load Dead Load	* * * * * * * * * * * * * * * * * * *	2245	LB
otal Load:	PT1=	4629	LB
_ocation:	X1=	2.6	FT
Properties For Select Structural- DOUGLAS FIR-LARCH (NORTH)	.	4000	DOL
Bending Stress:	Fb= Fv=	1300 95	PSI PSI
Shear Stress: Modulus of Elasticity:	E=	1900000	PSI
Stress Perpendicular to Grain	Fc_perp=	625	PSI
Adjusted Properties:			
Ebr⊬Tension).	Fb'=	1430	PSI
Adjustment Factors: Cd=1,00 Cf=1,10		05	DCI
Adjustment Factors: Cd=1.00	-v -	95	PSI
Design Requirements:			
Maximum Moment:	M=	5 807	FT-LB
2.6 FT From Left Support		2.00	
Shear (@ d from beam end):	V=	2422	LB
Comparisons With Required Sections: Section Modulus:	Srea=	48.8	IN3
Section Modulus:	S=	73.8	IN3
4rea.	Areq=	38.3	IN2
	. A=	39.3	IN2
Moment of Inertia:	req=	44.1	N4
Laving A Williams	l=	415.2	IN4
Variable Commence	,		
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A IV V	<i>3</i>		
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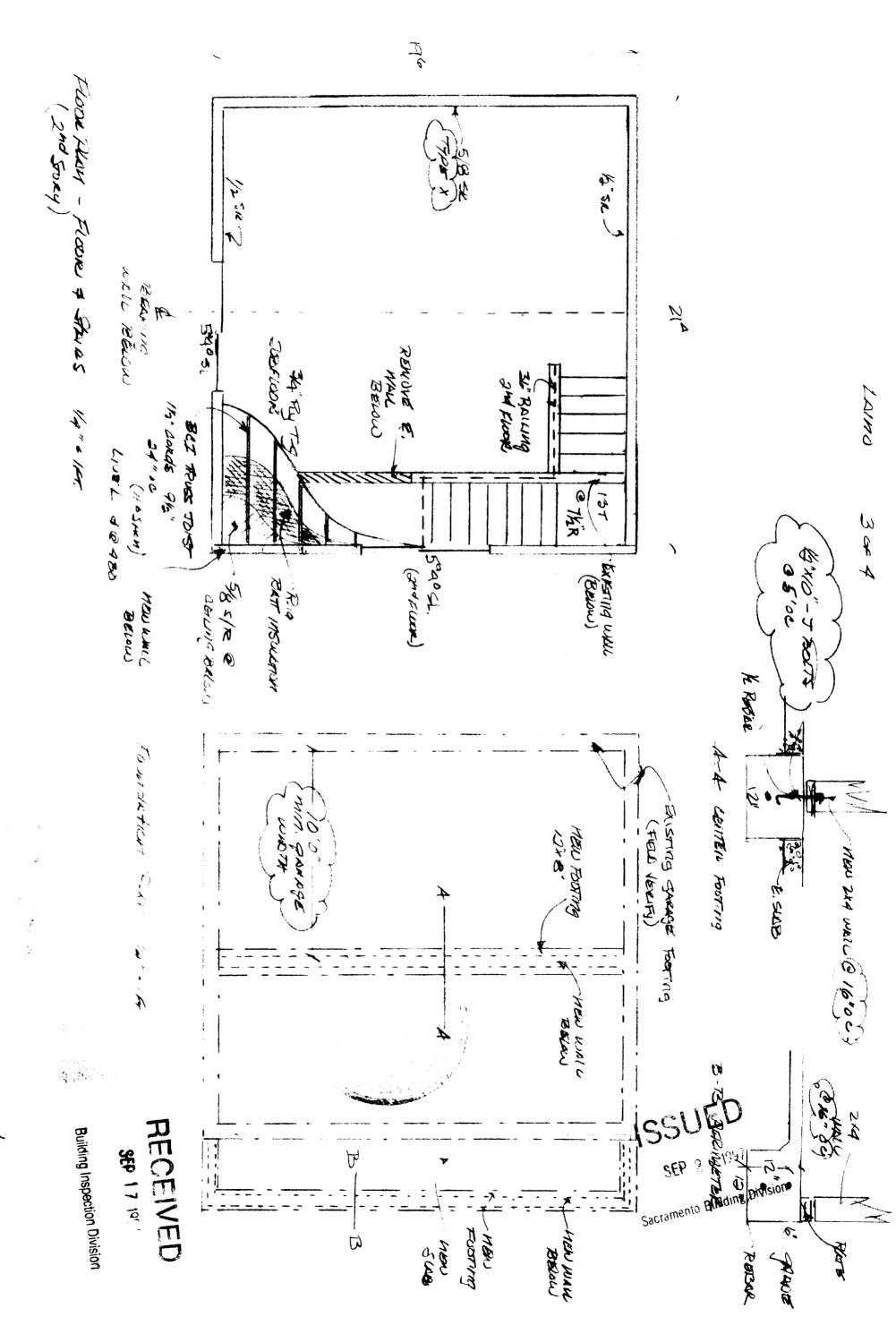
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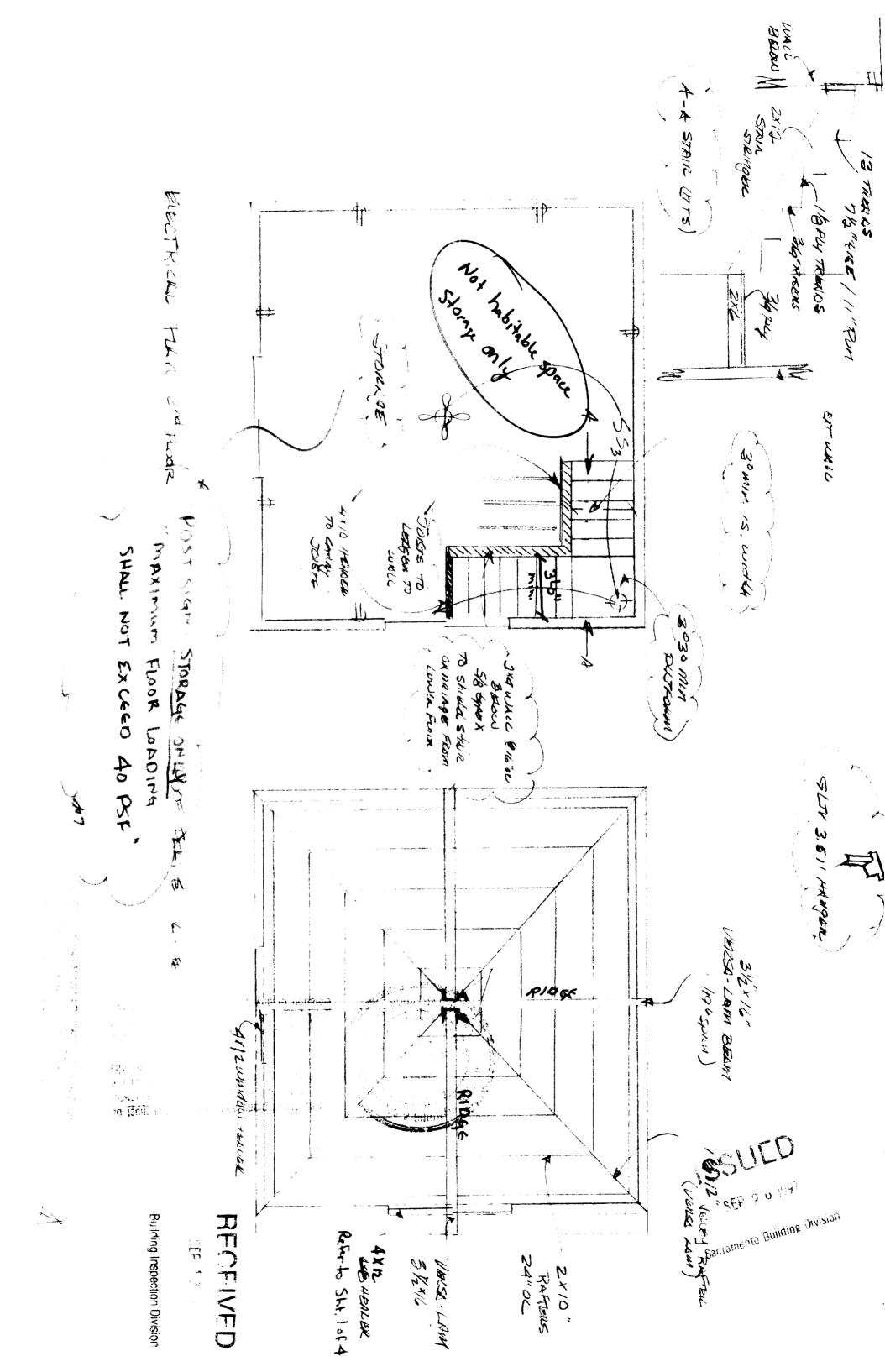
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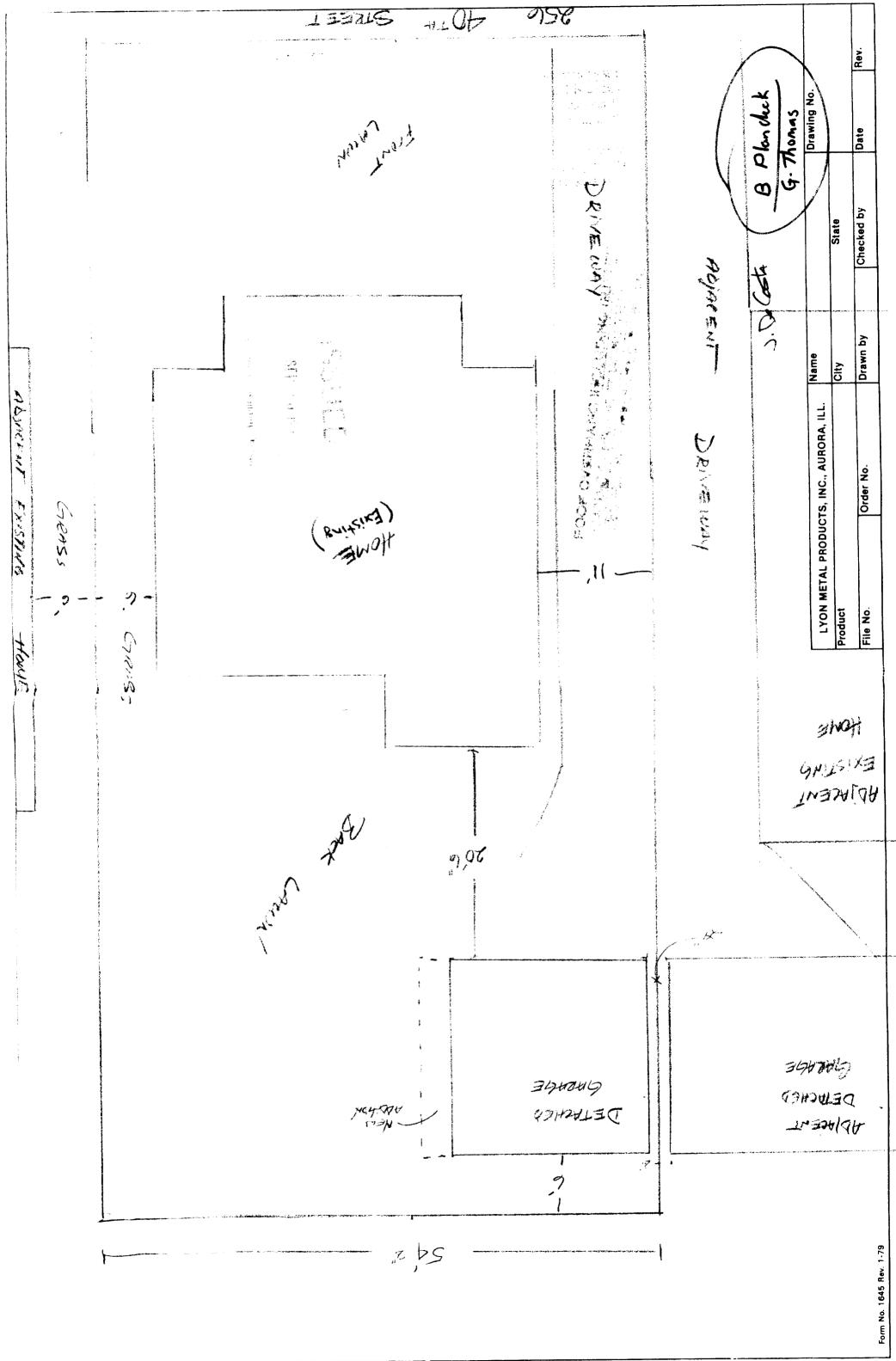
Building Inspection Division

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