

CITY OF SACRAMENTO  
1231 I Street, Sacramento, CA 95814

Permit No: 0014429  
Insp Area: 2

Site Address: 1 VIERRA CT SAC  
Parcel No: 031-0750-039

Sub-Type: RES  
Housing (Y/N): N

**CONTRACTOR**  
ZIMMERMAN ROOFING, INC  
3675 R STREET  
SACRAMENTO, CA 95816

**OWNER**  
ARAGON MARIA  
1 VIERRA CT  
SACRAMENTO CA 95831

**ARCHITECT**

Nature of Work: 27 SQ T/O REROOF W MONIER TILE

**CONSTRUCTION LENDING AGENCY:** I hereby affirm under penalty of perjury that there is a construction lending agency for the performance of the work for which this permit is issued (Sec. 3097, Civ. C).

Lender's Name \_\_\_\_\_ Lender's Address \_\_\_\_\_

**LICENSED CONTRACTORS DECLARATION:** I hereby affirm under penalty of perjury that I am licensed under provisions of Chapter 9 (commencing with section 7000) of Division 3 of the Business and Professions Code and my license is in full force and effect.

License Class C31 License Number 557559 Date 12-8-00 Contractor Signature Alma Gonzalez

**OWNER-BUILDER DECLARATION:** I hereby affirm under penalty of perjury that I am exempt from the contractors License Law for the following reason (Sec. 7031.5, Business and Professions Code; any city or county which requires a permit to construct, alter, improve, demolish, or repair any structure, prior to its issuance, also requires the applicant for such permit to file a signed statement that he or she is licensed pursuant to the provisions of the Contractors License Law (Chapter 9 (commencing with Section 7000) of Division 8 of the Business and Professions Code) or that he or she is exempt therefrom and the basis for the alleged exemption. Any violation of Section 7031.5 by any applicant for a permit subjects the applicant to a civil penalty of not more than five hundred dollars (\$500.00):

\_\_\_\_\_, I, as a owner of the property, or my employees with wages as their sole compensation, will do the work, and the structure is not intended or offered for sale (Sec. 7044, Business and Professional Code: The Contractors License Law does not apply to an owner of property who builds or improves thereon, and who does such work himself or herself or through his/her own employees, provided that such improvements are not intended or offered for sale. If, however, the building or improvement is sold within one year of completion, the owner-builder will have the burden of proving that he/she did not build or improve for the purpose of sale.)

\_\_\_\_\_, I, as owner of the property, am exclusively contracting with licensed contractors to construct the project (Sec. 7044, Business and Professions Code. The Contractors License Law does not apply to an owner of property who builds or improves thereon, and who contracts for such projects with a contractor(s) licensed pursuant to the Contractors License Law).

\_\_\_\_\_, I am exempt under Sec. \_\_\_\_\_ B & PC for this reason: \_\_\_\_\_

Date \_\_\_\_\_ Owner Signature \_\_\_\_\_

**IN ISSUING THIS BUILDING PERMIT,** the applicant represents, and the city relies on the representation of the applicant, that the applicant verified all measurements and locations shown on the application or accompanying drawings and that the improvement to be constructed does not violate any law or private agreement relating to permissible or prohibited locations for such improvements. This building permit does not authorize any illegal location of any improvement or the violation of any private agreement relating to location of improvements.

I certify that I have read this application and state that all information is correct. I agree to comply with all city and county ordinances and state laws relating to building construction and hereby authorize representative(s) of this city to enter upon the abovementioned property for inspection purposes.

Date 12-8-00 Applicant/Agent Signature Alma Gonzalez

**WORKER'S COMPENSATION DECLARATION:** I hereby affirm under penalty of perjury one of the following declarations:

\_\_\_\_\_, I have and will maintain a certificate of consent to self-insure for workers' compensation as provided for by Section 3700 of the Labor Code, for the performance of work for which the permit is issued.

I have and will maintain workers' compensation insurance, as required by Section 3700 of the Labor Code, for the performance of the work for which this permit is issued. My workers' compensation insurance carrier and policy number are:

Carrier PENNSYLVANIA GENERAL INSU. CO. Policy Number 713-00-2021 Exp Date 10/01/2001

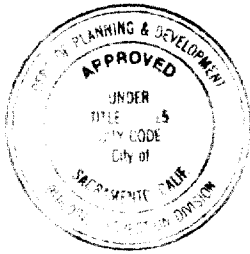
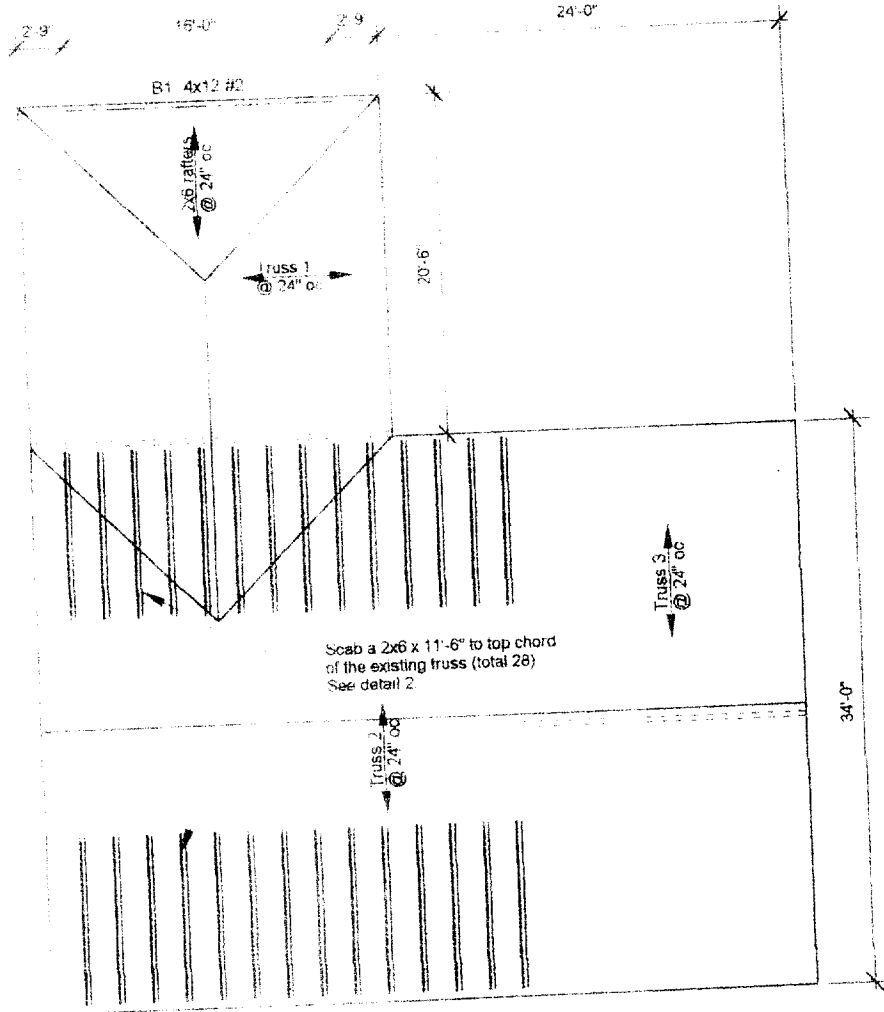
\_\_\_\_\_, (This section need not be completed if the permit is for \$100 or less) I certify that in the performance of the work for which this permit is issued, I shall not employ any person in any manner so as to become subject to the workers' compensation laws of California and agree that if I should become subject to the workers' compensation provisions of Section 3700 of the Labor Code, I shall forthwith comply with those provisions.

Date 12-8-00 Applicant Signature Alma Gonzalez

WARNING: FAILURE TO SECURE WORKER'S COMPENSATION COVERAGE IS UNLAWFUL AND SHALL SUBJECT AN EMPLOYER TO CRIMINAL PENALTIES AND CIVIL FINES UP TO ONE HUNDRED THOUSAND DOLLARS (\$100,000) IN ADDITION TO THE COST OF COMPENSATION, DAMAGES AS PROVIDED FOR IN SECTION 3706 OF THE LABOR CODE, INTEREST AND ATTORNEY'S FEE.

**THIS PERMIT SHALL EXPIRE BY LIMITATION IF WORK IS NOT COMMENCED WITHIN 180 DAYS.**

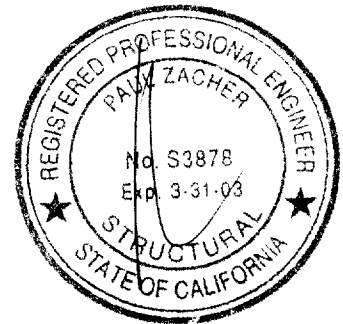
# 1 VIERRA CT.



This set of plans and specifications must be kept on the job at all times and it is unlawful to make any changes or alterations from the same without written permission from the Building Inspection Division.

The approval of this plan and specification SHALL NOT be held to permit or approve the violation of any City Ordinance or State Law.

REVIEWED BY: *[Signature]*  
12/5/00



Notes

1. This is a reroof project. The new roofing material shall be a Light Weight Concrete Tile. The tile shall weigh less than or equal to 7.0 psf.
2. All structural wood members that were observed appear to be in sound condition and without structural defect.



1

## ROOF PLAN - ARAGORN

Not to Scale 20

Scab 2x4 w/ 16d @ 12" oc  
staggered to top chord of  
existing truss.

Existing truss  
top chord

1'-0"  
min.

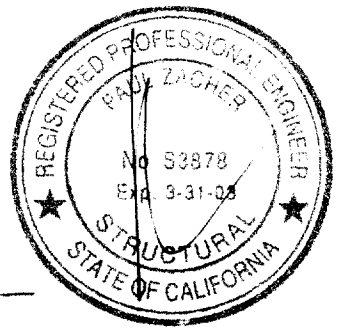
Existing bearing wall

Existing truss web

2

### TRUSS REINFORCEMENT DETAIL

scale: 1/2" = 1'-0"



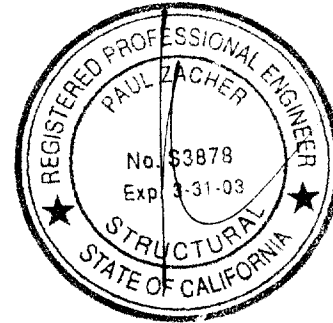
Aragorn

Paul Zacher - Structural Engineers  
4701 Lakeside Way  
Fair Oaks, CA 95628

TEL: 916.961.3960  
FAX: 916.961.6552

November 16, 2000

Zimmerman Roofing  
3675 R Street  
Sacramento, CA 95816  
TEL: 916.454.3667  
FAX: 916.455.3784



Attn: Mr. Jeff Tucker,

re. Job 2000\_308 ARAGON

Subject: Structural Investigation Report of the Roof for the Residence located at 1 Vierra Court,  
Sacramento, CA 95831.

As requested by Mr. Jeff Tucker, this is a report to determine what needs should be addressed to correct any structural deficiencies of the roof. Paul Zacher visited the site September 18, 2000. The investigation was made to determine the existing condition of the structure. All information, data and analysis contained within this report are based on the 1997 Uniform Building Code.

The following is based on visual observations with no subsurface investigation being made.

**DESCRIPTION:**

Type of Facility	Residence
Year Built	Estimated 1980's vintage
Occupancy	Residential
No. of Stories	One.
Dimensions	Approximately 2000 square feet with a first story plate height of 8 feet.

**CONSTRUCTION:**

Roof:  
The roof covering will consist of a Light Weight Concrete Tile over 1/2" solid sheathing. The living and garage areas are framed with wood pre-engineered trusses spaced at 24" on center.

**CONCLUSIONS:**

Roof:  
The living area lacks sufficient structural capacity for the applied live and dead loads. The garage has sufficient structural capacity for the applied live and dead loads.

1/2

Aragorn

Paul Zacher - Structural Engineers  
4701 Lakeside Way  
Fair Oaks, CA 95628

TEL: 916.961.3960  
FAX: 916.961.6552

RECOMMENDATIONS:

If any of the following recommendations do not correspond to actual field conditions, the engineer of record shall be notified for further investigation and evaluation before continuing work.

Living Area

1. Scab a 2x6 DF#2 x 11'-6" long rafter to the top chord of the existing truss. See details 1 and 2.

It shall be noted that small hairline cracking may occur at exterior stucco and interior gypboard finished walls that are load bearing or distributing roof strut loads. These cracks are a natural occurrence as the existing structure re-distributes the new roof weight. They are cosmetic in nature and are not an indication of a structural hazard or failure.

It shall be noted that some deflection of the rafters may be evident after installation of the tile. The existing roof framing has deflected but this may not be readily evident due to the uneven nature of the existing roofing material. Concrete tile is a very consistent and uniform product and when installed in an even plane, even small deflections can become apparent. This is only a cosmetic issue and not a structural concern.

The inspection consisted of visual observation only, made solely to determine the structural capacity of the existing roof. Analysis does not determine any effects on the overall structure under lateral forces or effects on the foundation unless specifically noted in the calculations and in this document. No warranties, expressed or implied, are made or intended in conjunction with this report. The inspection was made only to the portions that were accessible. The specific items noted were those that were observable and there may be defects that are not observable, or are hidden by architectural and structural materials.

If you have any questions on the above, do not hesitate to call.

Sincerely,



Paul Zacher, P.E., S.E.  
file

**DESIGN LOADING:**

Roof Pitch 4 in 12  
Pitch Adjustment Factor 1.05

**LOCATION: ROOF**

<u>MATERIAL</u>	<u>WEIGHT</u>	
Light Weight Tile	7.00	psf
Roofing felt	0.30	psf
1/2" OSB/ plywood	1.50	psf
1x4 skip sht'g	1.09	psf
2x6 rafters @ 24" oc	1.00	psf
	Load	10.9 psf
	Roof Pitch Adjustment	0.59 psf
	Total Load	11.5 psf

**LOCATION: TOP CHORD**

<u>MATERIAL</u>	<u>WEIGHT</u>	
Light Weight Tile	7.00	psf
Roofing felt	0.30	psf
1/2" OSB/ plywood	1.50	psf
1x4 skip sht'g	1.09	psf
2x4 truss @ 24" oc	0.64	psf
	Load	10.5 psf
	Roof Pitch Adjustment	0.57 psf
	Total Load	11.1 psf

**LOCATION: BOTTOM CHORD**

<u>MATERIAL</u>	<u>WEIGHT</u>	
Batt/blown insul	0.50	psf
2x4 truss @ 24" oc	1.28	psf
1/2" Gypboard	2.50	psf
	Load	4.3 psf

P K Zacher S E

4701 Lakeside Way  
Fair Oaks, CA 95628  
TEL: (916) 961-3960  
FAX: (916) 961-6552

Job #                     

Date: 11-16-00

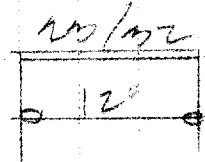
LOADING

2x FTR

2x 11' Spf - 2x 23' Spf

2x 16' Spf - 2x 13' Spf

2-6#2

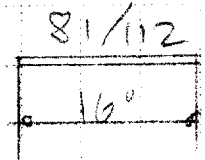


2x1

2x 11' Spf - 7' Spf 81' Spf

2x 16' Spf - 2x 13' Spf

4x12#2



Paul Zacher - Structural Engineers  
 4701 Lakeside Way  
 Fair Oaks  
 TEL: (916) 981-3960  
 FAX: (916) 981-6552

Title :  
 Dsgnr:  
 Description :  
 Scope :

Job #  
 Date: 6:26PM, 16 NOV 00

Rev: 510304  
 User: KW:0602844, Ver 9: 11: 22 Jun-1999 Win32  
 (c) 1983-99 ENERCALC

### Timber Beam & Joist

c:\enercalc\test.ecw.Calculations

Description RAFTERS AND BEAMS

#### Timber Member Information

Calculations are designed to 1997 NDS and 1997 UBC Requirements

	rafter	B1
Timber Section	2x6	4x12
Beam Width	in 1.500	3.500
Beam Depth	in 5.500	11.250
Le: Unbraced Length	ft 0.00	0.00
Timber Grade	Douglas Fir - Larch, Douglas Fir - Larch	
Fb - Basic Allow	psi 875.0	875.0
Fv - Basic Allow	psi 95.0	95.0
Elastic Modulus	ksi 1,600.0	1,600.0
Load Duration Factor	1.250	1.250
Member Type	Sawn	Sawn
Repetitive Status	Repetitive	No

#### Center Span Data

		12.00	16.00
Span	ft		
Dead Load	#/ft	23.00	81.00
Live Load	#/ft	32.00	112.00

#### Results

Ratio = 0.9607 0.8344

Mmax @ Center	in-k	11.88	74.11
@ X =	ft	6.00	8.00
f <sub>b</sub> Actual	psi	1,570.9	1,003.8
F <sub>b</sub> Allowable	psi	1,635.2	1,203.1
		Bending OK	Bending OK
f <sub>v</sub> Actual	psi	55.7	52.2
F <sub>v</sub> Allowable	psi	118.8	118.8
		Shear OK	Shear OK

#### Reactions

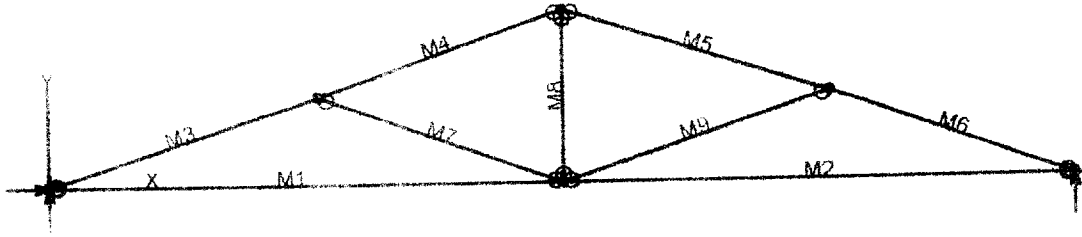
@ Left End	DL	lbs	138.00	648.00
	LL	lbs	192.00	896.00
	Max. DL+LL	lbs	330.00	1,544.00
@ Right End	DL	lbs	138.00	648.00
	LL	lbs	192.00	896.00
	Max. DL+LL	lbs	330.00	1,544.00

#### Deflections

Ratio OK Deflection OK

Center DL Defl	in	-0.322	-0.180
L/Defl Ratio		446.5	1,068.1
Center LL Defl	in	-0.449	-0.249
L/Defl Ratio		320.9	772.5
Center Total Defl	in	-0.771	-0.428
Location	ft	6.000	8.000
L/Defl Ratio		186.7	448.3





# VisualAnalysis 3.50.c Report

9/27/00 13:27:11

Project: Truss 1

File: D:\Program Files\IES\VA35\VA35.DWG

Company: PK Associates Engineers

Engineer: Paul Zacher

Result Units: Feet, Pounds, Degrees, Fahrenheit, Seconds.

## Nodes

Node	X ft	Y ft	Fix	DX	Fix	DY	Fix	RZ
11	0.00	0.00	Yes	Yes	Yes	No		
12	10.50	0.00	No	No	No			
13	01.00	0.00	No	No	Yes			
14	5.00	1.83	No	No	No			
15	16.00	1.83	No	No	No			
16	10.50	3.58	No	No	No			

## Member Elements

Member	Section	Material	Length ft
M1	SS2x4	Wood	10.50
M2	"	"	10.50
M3	"	"	5.80
M4	"	"	5.30
M5	"	"	5.77
M6	"	"	5.27
M7	"	"	5.00
M8	"	"	3.50
M9	"	"	5.80

## Section Properties

Category	Section	Ax in <sup>2</sup>	Iz in <sup>4</sup>	Sy+ in <sup>3</sup>	Sy- in <sup>3</sup>
Wood	Sha SS2x4	5.25	5.36	3.06	3.06

## Material Properties

Material	Strength psi	Elasticity psi	Poisson	Density lb/ft <sup>3</sup>
Wood	NA	1700000.00	0.16	40.47

## Load Combination Summary

Equation Case: Equation Case 1  
 Combination: +1D+1L+1LF  
 Contributing Cases & Source  
 Service Case 1 (Dead loads)  
 Service Case 1 (Roof Live loads)

## Member Uniform Loads

Check the results to state, or report properties.

## Nodal Reactions

Node	Load Case	FX lbs	FY lbs	MZ lb-ft
1	Equation Case 1	0.00	659.40	-NA-
2		-NA-	659.40	-NA-

## Member Results

Member	Axial lbs	Vy lbs	Mz lb-ft	Dy in
4	1513.21	84.78	-101.16	-0.1210
	1513.21	-24.68	37.6447	-0.1743
	1513.21	5.4154	71.3658	-0.1598
	<b>1513.21</b>	35.5154	0.0000	0.0000
M	1421.98	35.52	0.0000	-0.0000
	1421.98	-5.4154	71.3658	-0.1599
	1421.98	34.6846	37.6447	0.1742
	1421.98	54.7846	-101.16	0.1210
M	<b>-1632.78</b>	114.24	0.0000	-0.0000
	-1601.41	19.9559	<b>129.19</b>	-0.1087
	-1570.04	-74.33	76.6807	-0.1267
	-1538.67	168.61	-157.58	-0.1209
M	-1109.83	<b>157.64</b>	-157.58	-0.1207
	-1078.79	73.3785	45.1228	-0.1497
	-1049.94	-12.88	97.6509	-0.1592
	-1020.10	-98.15	0.0000	-0.1183
M	-1098.45	<b>-169.81</b>	<b>-160.30</b>	-0.0989
	-1068.22	-75.12	74.8512	-0.1564
	-1038.19	19.5713	128.28	-0.1717
	-1008.06	114.26	0.0000	-0.1077
I	-1549.08	-97.14	-0.0000	0.0142
	-1518.71	-12.31	96.7464	-0.0625
	-1487.68	72.5216	43.3135	-0.0890
	-1456.64	157.35	-160.30	-0.0969
	-551.56	0.0000	0.0000	-0.1063
	-551.56	0.0000	0.0000	-0.1049
	-551.56	0.0000	0.0000	-0.1036
	-551.56	0.0000	0.0000	-0.1022
	441.12	-0.0000	0.0000	-0.0219
	441.12	0.0000	-0.0000	-0.0204
	441.12	-0.0000	-0.0000	-0.0194
	441.12	-0.0000	-0.0000	-0.0185
	-449.72	-0.0000	0.0000	-0.1215
	-449.72	-0.0000	-0.0000	-0.1166
	-449.72	-0.0000	-0.0000	-0.1117
	-449.72	-0.0000	-0.0000	-0.1067

### **BENDING & COMP: TRUSS 1 - MEMBER 3**

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

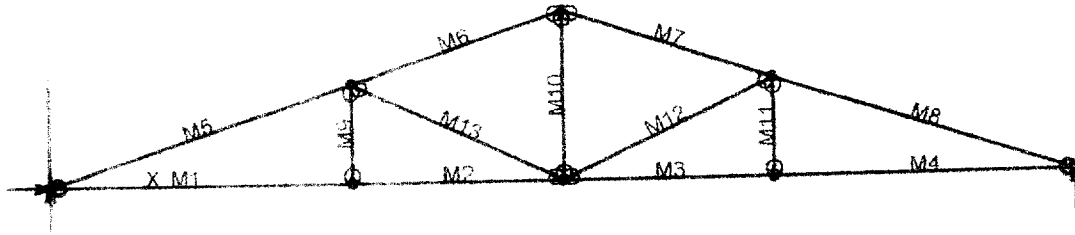
#### Grading:

1x or 4x                      Doug-fir larch No. 2

#### Assumptions:

Solid sheathing on top chord of truss. Therefore,  
continuous lateral support is provided along compression face  
Maximum center-center spacing = 24"

Width, b	3.5 inches
Depth, d	3.5 inches
Length	5.8 feet
Max Axial Comp. C	1538 lbs
Max Reaction, R	168 lbs
Max Moment, M	157 ft-lbs
Max LL Deflection	0.04 inches
Max TL Deflection	0.02 inches
LL Defl Criteria = L/240	240
TL Defl Criteria = L/380	380
Duration factor, Cd	1.25
Repetitive Factor, Cr	1.15
Size Factor, Cf bending	1.5    1.5 for 2x4, 1.3 for 2x6
Size Factor, Cf comp	1.15    1.15 for 2x4, 1.1 for 2x6
Buckling Factor, CT	1.16
Fc	293 psi
Fcc	1496 psi
Fcx	2084 psi
Fcy	1184 psi
Fb	615 psi
F'b=Fb*	2156 psi
Shear D/C ratio	0.40 < 1.0, Member OK
Interaction equation:	
(fc/Fc) <sup>2</sup> +	
fb/(F'b(1-fc/Fcc)) =	0.42 < 1.0, Member OK
Live Load defl ratio	0.14 < 1.0, Member OK
Total Load defl ratio	0.31 < 1.0, Member OK



# VisualAnalysis 3.50 c Report

1998-09-13 13:32:07

Project: Truss 2

File: C:\Program Files\IES\VA35\Truss 2.rdb

Company: PK Associates Engineers

Engineer: Paul Eicher

Units: Feet Pounds Degrees Fahrenheit Seconds

## Nodes

Node	X ft	Y ft	Y Fix	DX Fix	DY Fix	RZ Fix
1	0.00	0.00	Yes	Yes	No	No
2	10.00	0.00	No	No	No	No
3	17.00	0.00	No	No	No	No
4	24.00	0.00	No	No	No	No
5	34.00	0.00	No	Yes	No	No
6	10.00	3.33	No	No	No	No
7	24.00	3.33	No	No	No	No
8	17.00	3.67	No	No	No	No

## Member Elements

Member	Section	Material	Length ft
4	SS2x4	Wood	10.00
M	"	"	7.00
K	"	"	7.00
H	"	"	10.00
M	"	"	10.54
K	"	"	7.08
M	"	"	7.38
M	"	"	10.54
M	"	"	3.33
M	"	"	3.67
M	"	"	3.33
M	"	"	7.38
M	"	"	7.38

## Section Properties

Category	Section	Ax in <sup>2</sup>	Ix in <sup>4</sup>	Sy+ in <sup>3</sup>	Sy- in <sup>3</sup>
Wood	Sha SS2x4	5.25	5.36	3.06	3.06

## Material Properties

Material	Strength psi	Elasticity psi	Poisson	Density lb/ft <sup>3</sup>
Wood	NA	1700000.00	0.36	40.47

## Load Combination Summary

Equation Case: Equation Case 1  
 Combination: 1D+1L+1LR  
 Contributing Cases & Source

Service Case 1 Dead loads  
 Service Case 2 Wind Live 10000

## Member Uniform Loads

If this item is empty, check the selection state, or report properties.

## Nodal Reactions

Node	Load Case	FX lbs	FY lbs	MZ lb-ft
1	Equation Case 1	0.00	1067.60	-NA-
2	"	-NA-	1067.60	-NA-

## Member Results

Member	Axial lbs	Vy lbs	Mz lb-ft	Dy in
41	2430.63	-48.09	-50.90	-0.3299
42	2430.63	19.42	61.3853	-0.3447
43	2430.63	9.2436	78.3509	-0.2465
44	<b>2430.63</b>	89.9103	0.0000	-0.0000
45	2430.63	-26.19	-23.55	-0.3413
46	2430.63	-6.1266	14.0398	-0.3449
47	2430.63	13.9400	4.9236	-0.3380
48	2430.63	34.0067	-50.90	-0.3299
49	2430.63	-34.01	-50.90	-0.3299
50	2430.63	-13.94	4.9236	-0.3380
51	2430.63	6.1266	14.0391	-0.3449
52	2430.63	26.1933	-23.55	-0.3413
53	2430.63	37.91	0.0000	-0.0000
54	2430.63	-9.2436	78.3509	-0.2465
55	2430.63	19.4231	61.3853	-0.3446
56	2430.63	48.0897	-50.90	-0.3298
57	<b>-2631.45</b>	209.01	0.0000	0.0000
58	-2574.37	37.5927	<b>431.68</b>	<b>-0.8741</b>
59	-2517.23	-133.82	262.64	-0.8551
60	-2460.21	<b>-305.23</b>	<b>-507.11</b>	-0.3353
61	-1775.00	248.62	-507.11	-0.3353
62	-1734.91	-128.68	-43.72	-0.3225
63	-1694.81	8.7360	125.31	-0.3867
64	-1654.71	-111.21	0.0000	-0.3552
65	-1775.00	-248.62	-507.11	-0.3000
66	-1734.91	-128.68	-43.72	-0.2873
67	-1694.81	8.7360	125.31	-0.3515
68	-1654.72	111.21	0.0000	-0.3000
69	<b>-2631.45</b>	-209.01	0.0000	0.3351
70	-2574.37	-37.59	431.68	-0.8391
71	-2517.23	133.82	262.64	-0.8198
72	-2460.21	<b>305.23</b>	<b>-507.11</b>	-0.3002
73	82.0964	-0.0000	-0.0000	0.0307
74	82.0964	-0.0000	-0.0000	0.0457
75	82.0964	-0.0000	-0.0000	0.0587
76	82.0964	-0.0000	0.0000	0.0717
77	838.29	-0.0000	0.0000	0.0556
78	838.29	0.0000	-0.0000	0.0556
79	838.29	-0.0000	-0.0000	0.0556
80	838.29	0.0000	-0.0000	0.0556
81	82.0964	0.0000	0.0000	0.0394
82	82.0964	0.0000	0.0000	0.0524
83	82.0964	0.0000	0.0000	0.0654
84	82.0964	0.0000	0.0000	0.0784

11	914.72	0.0000	0.0000	0.2144
12	914.72	0.0000	-0.0000	0.3004
13	914.72	0.0000	-0.0000	0.3000
14	914.72	0.0000	-0.0000	0.3321
15	914.72	0.0000	0.0000	0.2088
16	914.72	0.0000	0.0000	0.2087
17	914.72	0.0000	0.0000	0.2185
18	914.72	0.0000	0.0000	0.2143



## BENDING & COMP: TRUSS 2 - MEMBER 5

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

### Grading:

2x or 4x

Doug-fir larch No. 2

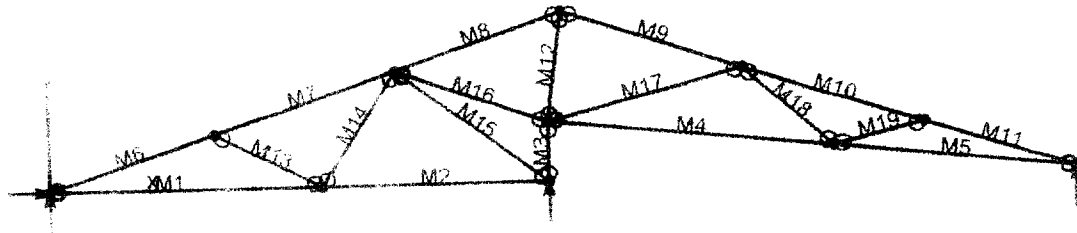
### Assumptions:

Solid sheathing on top chord of truss. Therefore,

continuous lateral support is provided along compression face

Maximum center-center spacing = 24"

Width, b	5.5 inches
Depth, d	8.5 inches
Length	10.54 feet
Max Axial Comp. C	2460 lbs
Max Reaction, R	305 lbs
Max Moment, M	507 ft-lbs
Max LL Deflection	0.14 inches
Max TL Deflection	0.33 inches
LL Defl Criteria = L	240
TL Defl Criteria = L	380
Duration factor, Cd	1.25
Repetitive Factor, Cr	1.15
Size Factor, Cf bending	1.5 (1.5 for 2x4, 1.3 for 2x6)
Size Factor, Cf comp	1.15 (1.15 for 2x4, 1.1 for 2x6)
Buckling Factor, CT =	1.29
fc =	298 psi
Fce =	1244 psi
Fb* =	2084 psi
Fc =	1038 psi
Fb =	804 psi
F'b = F'b* =	2156 psi
Shear D/C ratio	0.47 < 1.0, Member OK
Interaction equation (fc/Fc)^2 +	
(F'b/(F'b(1-fc/Fce))) =	0.57 < 1.0, Member OK
Live Load defl ratio	0.27 < 1.0, Member OK
Total Load defl ratio	0.47 < 1.0, Member OK



# VisualAnalysis 3.50.c Report

07/19/00 13:48:47

Project: Truss 3

File: Untitled.Vag

Company: PK Associates Engineers

Engineer: Paul Zacher

Units: Feet, Pounds, Degrees, Fahrenheit, Seconds.

## Nodes

Node	X ft	Y ft	Fix	DX	Fix	DY	Fix	RZ
1	0.00	0.00	Yes	Yes	No			
2	9.00	0.00	No	No				
3	18.50	0.00	"	Yes				
4	18.50	2.00	"	No				
5	26.00	0.97	"					
6	34.00	0.00	"	Yes				
7	5.50	1.83	"	No				
8	11.50	1.83	"					
9	17.00	5.57	"					
10	23.00	1.57	"					
11	29.00	1.57	"					

## Member Elements

Member	Section	Material	Length ft
M1	SS2x4	Wood	9.00
M2	"	"	1.50
M3	"	"	2.00
M4	"	"	9.00
M5	"	"	8.00
M6	"	"	5.00
M7	"	"	9.00
M8	"	"	5.00
M9	"	"	6.00
M10	"	"	4.00
M11	"	"	5.00
M12	"	"	3.00
M13	"	"	1.00
M14	"	"	4.57
M15	"	"	5.57
M16	"	"	3.00
M17	"	"	5.00
M18	"	"	1.04
M19	"	"	3.00

## Section Properties

Category	Section	Ax in <sup>2</sup>	Ix in <sup>4</sup>	Sy+ in <sup>3</sup>	Sy- in <sup>3</sup>
Wood	Sna SS2x4	5.25	5.38	3.06	3.06

## Material Properties

Material	Strength psi	Elasticity psi	Poisson	Density lb/ft <sup>3</sup>
Wood				

## Load Combination Summary

Equation Case: Equation Case 1  
 Combination: +1D+1L+1Lr  
 Contributing Cases & Source  
 Service Case 1 (Dead loads)  
 Service Case 2 (Roof Live loads)

## Member Uniform Loads

-----  
 This item is empty. Check the selection state, or report properties.  
 -----

## Nodal Reactions

Node	Load Case	FX lbs	FY lbs	MZ lb-ft
N1	Equation Case 1	-0.00	314.04	-NA-
N2	"	-NA-	1464.06	-NA-
N3	"	-NA-	357.10	-NA-

## Member Results

Member	Axial lbs	Vy lbs	Mz lb-ft	Dy in
12	494.74	-46.61	-71.19	-0.0162
13	494.74	-20.81	29.7493	-0.0647
14	494.74	4.9905	53.4779	-0.0723
15	494.74	30.7905	0.0000	-0.0000
16	-94.24	-22.76	0.0000	-0.0000
17	-94.24	-11.2586	29.8870	-0.0262
18	-94.24	20.2414	6.1584	-0.0223
19	-94.24	41.7414	-71.19	-0.0162
20	-1513.48	0.0000	0.0000	-0.0050
21	-1513.48	0.0000	0.0000	-0.0004
22	-1513.48	0.0000	0.0000	0.0042
23	-1513.48	0.0000	0.0000	0.0089
24	121.55	-47.67	-67.41	-0.0832
25	124.49	-20.59	41.0807	-0.1370
26	127.42	6.4825	63.5520	-0.1252
27	130.36	33.5572	0.0000	-0.0050
28	1039.82	-25.78	0.0000	0.0007
29	1043.58	-3.0178	38.5314	-0.0629
30	1045.34	19.7488	16.0601	-0.0907
31	1048.10	42.5153	-67.41	-0.0832
32	-558.86	112.57	0.0000	-0.0000
33	-527.49	18.2857	125.96	-0.0737
34	-496.12	-76.00	70.2061	-0.0690
35	-464.75	170.28	-167.27	-0.0250
36	-154.36	151.21	-167.27	-0.0250
37	-120.08	48.3722	42.5696	-0.0382
38	-85.80	-54.47	36.1473	-0.0304
39	-51.52	157.30	-186.53	-0.0069
40	970.85	173.51	-186.53	-0.0069
41	1002.37	79.2796	57.3614	-0.0525
42	1033.90	-14.95	119.54	-0.0698
43	1065.42	109.19	0.0000	-0.0121
44	843.22	-187.17	-208.18	-0.0615
45	877.50	-84.33	77.4741	-0.1135

	911.77	11.031	146.87	0.0000	0.0000
	946.08	11.34	0.0000	0.0000	0.0079
M	585.87	40.82	-123.21	0.0000	0.0003
	-531.31	27.99	84.7160	0.0000	0.0000
	-497.07	88.8506	36.3997	0.0000	0.0049
	-862.74	187.69	-208.18	0.0000	0.0000
X	1126.71	109.15	0.0000	0.0000	0.0018
	-1098.09	-19.46	109.10	0.0000	0.0075
	-1069.47	46.2159	48.0222	0.0000	0.0002
	1040.86	151.90	-123.21	0.0000	0.0003
M	863.75	0.0000	0.0000	0.0000	0.0083
	-863.75	0.0000	0.0000	0.0000	0.0028
	-863.75	0.0000	0.0000	0.0000	0.0027
	-863.75	0.0000	0.0000	0.0000	0.0081
M	-446.99	0.0000	0.0000	0.0000	0.0002
	-446.99	0.0000	0.0000	0.0000	0.0073
	-446.99	0.0000	0.0000	0.0000	0.0145
	-446.99	0.0000	0.0000	0.0000	0.0116
M	352.84	0.0000	0.0000	0.0000	0.0139
	352.84	0.0000	-0.0000	0.0000	0.0100
	352.84	0.0000	-0.0000	0.0000	0.0082
	352.84	0.0000	-0.0000	0.0000	0.0024
M	118.71	0.0000	0.0000	0.0000	0.0079
	118.71	0.0000	0.0000	0.0000	0.0043
	118.71	0.0000	0.0000	0.0000	0.0006
	118.71	0.0000	0.0000	0.0000	0.0031
M	-1039.04	0.0000	0.0000	0.0000	0.0085
	-1039.04	0.0000	0.0000	0.0000	0.0079
	-1039.04	0.0000	0.0000	0.0000	0.0074
	-1039.04	0.0000	0.0000	0.0000	0.0069
M	-1017.12	0.0000	0.0000	0.0000	0.0611
	-1017.12	0.0000	0.0000	0.0000	0.0413
	-1017.12	0.0000	0.0000	0.0000	0.0215
	-1017.12	0.0000	0.0000	0.0000	0.0017
M	492.45	0.0000	0.0000	0.0000	0.0714
	492.45	0.0000	0.0000	0.0000	0.0641
	492.45	0.0000	0.0000	0.0000	0.0568
	492.45	0.0000	0.0000	0.0000	0.0495
M	-557.94	0.0000	-0.0000	0.0000	0.0837
	-557.94	0.0000	-0.0000	0.0000	0.0812
	-557.94	0.0000	-0.0000	0.0000	0.0787
	-557.94	0.0000	0.0000	0.0000	0.0760

### BENDING & COMP: TRUSS 3 - MEMBER 11

Design based on 1997 UBC 2321 Division V and ANSUTPI 1-1995

#### Grading

2x or 4x

Doug-fir larch No. 2

#### Assumptions:

Solid sheathing on top chord of truss. Therefore,  
continuous lateral support is provided along compression face  
Maximum center-center spacing = 24"

Width, b	1.5 inches
Depth, d	3.5 inches
Length	5.27 feet
Max Axial Comp. C	1040 lbs
Max Reaction, R	153 lbs
Max Moment, M	123 ft-lbs
Max LL Deflection	0.04 inches
Max TL Deflection	0.09 inches
LL Defl Criteria = L <sub>v</sub>	240
TL Defl Criteria = L <sub>v</sub>	180
Duration factor, C <sub>d</sub>	1.25
Repetitive Factor, C <sub>r</sub>	1.15
Size Factor, C <sub>f</sub> bending	1.5 1.5 for 2x4, 1.3 for 2x6
Size Factor, C <sub>f</sub> comp	1.15 1.15 for 2x4, 1.1 for 2x6
Buckling Factor, C <sub>T</sub> =	1.15
E =	198 psi
F <sub>ce</sub> =	1789 psi
F <sub>c</sub> * =	2084 psi
F <sub>v</sub> =	1326 psi
f <sub>b</sub> =	482 psi
F <sub>b</sub> * = F <sub>b</sub> * =	2156 psi
Shear D/C ratio	0.36 < 1.0, Member OK
Interaction equation	
$(f_c/F_c)^2 +$	
$f_b/(F_b(1-f_c/F_{ce})) =$	0.27 < 1.0, Member OK
Live Load defl ratio	0.15 < 1.0, Member OK
Total Load defl ratio	0.26 < 1.0, Member OK