### **CITY OF SACRAMENTO** 1231 I Street, Sacramento, CA 95814

Permit No: 0406549

Insp Area:

2

Thos Bros:

317A7

Site Address: 1080 SILVER LAKE DR SAC

Parcel No: 029-0480-004

Sub-Type: REP

**CONTRACTOR** 

Housing (Y/N): N

ZIMMERMAN REROOFING CO. 3675 R ST

The same of the sa

**OWNER** TY MATT ARCHITECT

\$ACRAMENTO CA 95816

1080 SILVER LAKE DR SACRAMENTO CA 95831

CONSTRUCTION LENDI the work for which this permit is	NG AGENCY: I hereby affirm under penalty of perjury that there is a construction lending agency for the performance of issued (Sec. 3097, Civ. C).
Lender's Name	Lender's Address
(commencing with section 7000)	ORS DECLARATION: I hereby affirm under penalty of perjury that I am licensed under provisions of Chapter 9 of Division 3 of the Business and Professions Code and my license is in full force and effect.
License Class License	Number 763169 Date 428-04 Contractor Signature Kot.
reason (Sec. 7031.5, Business an prior to its issuance, also requires License Law (Chapter 9 (comme.	ARATION: I hereby affirm under penalty of perjury that I am exempt from the contractors License Law for the following d Professions Code; any city or county which requires a permit to construct, alter, improve, demolish, or repair any structure, the applicant for such permit to file a signed statement that he or she is licensed pursuant to the provisions of the Contractors acing with Section 7000) of Division 8 of the Business and Professions Code) or that he or she is exempt therefrom and the Any violation of Section 7031.5 by any applicant for a permit subjects the applicant to a civil penalty of not more than five
sale (Sec. 7044, Business and Pro who does such work himself or h	rty, or my employees with wages as their sole compensation, will do the work, and the structure is not intended or offered for offessional Code: The Contractors License Law does not apply to an owner of property who builds or improves thereon, and erself or through his/her own employees, provided that such improvements are not intended or offered for sale. If, however, old within one year of completion, the owner-builder will have the burden of proving that he/she did not build or improve for
The Contractors License Law doe licensed pursuant to the Contractor	
I am exempt under Sec	B & PC for this reason:
Date	Owner Signature
measurements and locations show private agreement relating to peri	PERMIT, the applicant represents, and the city relies on the representation of the applicant, that the applicant verified all vn on the application or accompanying drawings and that the improvement to be constructed does not violate any law or nissible or prohibited locations for such improvements. This building permit does not authorize any illegal location of any private agreement relating to location of improvements.
building construction and herby a	cation and state that all information is correct. I agree to comply with all city and county ordinances and state laws relating to athorize representative(s) of this city to enter upon the abovementioned property for inspection purposes.
Date 4-28-04	Applicant/Agent Signature Kati Cy
I have and will maintain a performance of work for which th  I have and will maintain w	orkers compensation insurance, as required by Section 3700 of the Labor Code, for the performance of the work for which
this permit is issued. My workers	compensation insurance carrier and policy number are:
Carrier STATE FUNI	Policy Number 713-0002021 Exp Date 10/01/2004
not employ any negson in airy man	completed if the pormit is for \$100 or less) I certify that in the performance of the work for which this permit is issued, Ishall the person as to become subject to the workers' compensation laws of California and agree that if I should become subject to the of Section 3700 of the Labor Code, I shall forthwith comply with those provisions.
Date 4-28-04	Applicant Signature Ket Cop
CRIMINAL PENALTIES AND	CURE WORKER'S COMPENSATION COVERAGE IS UNLAWFUL AND SHALL SUBJECT AN EMPLOYER TO CIVIL FINES UP TO ONE HUNDRED THOUSAND DOLLARS (\$100,000) IN ADDITION TO THE COST OF AS PROVIDED FOR IN SECTION 3706 OF THE LABOR CODE, INTEREST AND ATTORNEY'S FEE.

THIS PERMIT SHALL EXPIRE BY LIMITATION IF WORK IS NOT COMMENCED WITHIN 180 DAYS.

#### Matt

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Paul Zacher – Structural Engineers, Inc 4701 Lakeside Way Fair Oaks, CA 95628

TEL: 916.961.3960 FAX: 916.961.6552

April 17, 2004

Zimmerman Roofing 3675 R Street Sacramento, CA 95816

TEL: (916) 454-3667 FAX: (916) 691-1943

Attn.: Mr. Jeff Tucker,

re: Job 2004168: MATT

Subject: Structural Investigation Report of the Roof for the Residence located at 1080 Silver Lake Drive, Sacramento, CA 95831.

As requested by Mr. Jeff Tucker, this is a report to determine what needs should be addressed to correct any structural deficiencies of the roof. Paul Zacher visited the site April 16, 2004. The investigation was made to determine the existing condition of the structure. All information, data and analysis contained within this report are based on the 1997 Uniform Building Code with 2001 CBC Title 24 Amendments.

The following is based on visual observations with no subsurface investigation being made.

DESCRIPTION:

Residence. Type of Facility:

Year Built:

Estimated 1980's vintage.

Occupancy:

Residential.

No. of Stories:

One.

Dimensions:

Approximately 2000 square feet.

500.

#### CONSTRUCTION:

The roof covering will consist of a Standard Weight Concrete Tile over 7/16" solid sheathing. The roof structure is framed with pre-engineered wood trusses spaced at 24" on center.

**CONCLUSIONS:** 

Roof:

The roof structure currently lacks sufficient structural capacity for the applied live and dead loads. See "Recommendations" for location and repair to bring the roof structure up to the required capacity."



Paul Zacher - Structural Engineers, Inc 4701 Lakeside Way Fair Oaks, CA 95628

TEL: 916.961.3960 FAX: 916.961.6552

### **RECOMMENDATIONS:**

If any of the following recommendations do not correspond to actual field conditions, the engineer of record shall be notified for further investigation and evaluation before continuing work. Roof Structure:

1. Scab a 1 3/4" x 11 1/4" LVL to the existing header. See details 1 and 2.

It shall be noted that small hairline cracking may occur at exterior stucco and interior gypboard finished walls that are load bearing or distributing roof strut loads. These cracks are a natural occurrence as the existing structure re-distributes the new roof weight. They are cosmetic in nature and are not an indication of a structural hazard or failure.

It shall be noted that some deflection of the rafters may be evident after installation of the tile. The existing roof framing has deflected but this may not be readily evident due to the uneven nature of the existing roofing material. Concrete tile is a very consistent and uniform product and when installed in an even plane, even small deflections can become apparent. This is only a cosmetic issue and not a structural concern.

The inspection consisted of visual observation only, made solely to determine the structural capacity of the existing roof. Analysis does not determine any effects on the overall structure under lateral forces or effects on the foundation unless specifically noted in the calculations and in this document. No warranties, expressed or implied, are made or intended in conjunction with this report. The inspection was made only to the portions that were accessible. The specific items noted were those that were observable and there may be defects that are not observable, or are hidden by architectural and structural materials.

If you have any questions on the above, do not hesitate to call.

Sincerely,

Paul Zacher, P.E., S.E.

file

### **DESIGN LOADING:**

Roof Pitch	4	in 12
Pitch Adjustment Factor	1.05	

The dead and live load on truss top chord is placed along the length of the top chord.
Therefore, the live load is as follows:

Live Load on top chord 15.2

# LOCATION: TOP CHORD

MATERIAL	WEIGHT	-	
Standard Weight Tile		10.30	psf
Roofing felt		0.30	psf
7/16" OSB/ plywood		1.30	psf
1x4 skip sht'g		1.09	psf
2x4 truss @ 24" oc		<u>0.64</u>	psf
<del>.</del>	Total Load	13.6	psf

### **LOCATION: BOTTOM CHORD**

MATERIAL		<u>WEIGH</u>	<u>r</u>
Batt/blown insul		0.50	psf
2x4 truss @ 24" oc		1.28	psf
1/2" Gypboard		<u>2.50</u>	psf
-, J.F. 1	Load	4.3	psf

4701 Lakside Way PAUL ZACHER- STRUCTURAL ENGINEERS, INC. Fair Oaks, Ca 95628 Job #: 04\_168 TEL: (916) 961-3960 FAX: (916) 961-3938 Date: 04/17/2004 LOADING: 322 / 288 B1:\_\_\_\_ 7'-0" 4x12 #2 Dr = 17.9 psf x 18'-0" = 322 plfLr = 16.0 psf x 18'-0" = 288 plf197 / 176 B2:\_\_\_\_ 4x12 #2 + 1-3/4"x11-1/4" LVL Dr = 17.9 psf x 11'-0" = 197 plf16'-0" Lr = 16.0 psf x 11'-0" = 176 plf

Paul Zacher - Structural Engr's

4701 Lakeside Way Fair Oaks, CA 95628 TEL: (916) 961-3960

FAX: (916) 961-6552

Title : Dsgnr: Description :

Job# Date: 6:21PM, 17 APR 04

Scope:

Rev: 560100 User: KW-0602844, Ver 5.6.1, 25-Oct-2002 (c)1983-2002 ENERCALC Engineering Software

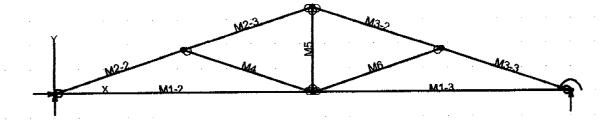
### **Timber Beam & Joist**

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Description

RAFTERS AND BEAMS

Timber Member Information		ATT - LABORATO -	Calculations are designed to 1997 NDS and 1997 UBC Requirements	
		B1	B2	
Timber Section		4x12	4x12#2 + 1	
Beam Width	in	3,500	5.250	
Beam Depth	in	11.250	11.250	
Le: Unbraced Length	ft	0.00	0.00	
Timber Grade			ustom, DF#2 + LVL	
Fb - Basic Allow	psi	1,000.0	1,450.0	
Fv - Basic Allow	psi	95.0	158.0	
Elastic Modulus	ksi	1,700.0	1,666.7	
Load Duration Factor		1,250	1.250	Α.
Member Type		Sawn	Manuf/Pine	
Repetitive Status		No	No	
Center Span Data			tali NESI in in an anto the common through the sales of the control of the contro	
Span	ft	7.00	16.00	THE COLUMN STREET SECTION STREET, COLUMN STREET, CO
Dead Load	#/ft	322.00	197.00	
Live Load	#/ft	288.00	176.00	
Results	Ratio =	0.5041	0.7136	
Mmax @ Center	in-k	44.83	143.23	
@ X =	ft.	3,50	8.00	
=		607.3	1,293.4	
fb : Actual Fb : Allowable	psi	1.375.0	1.812.5	
rb . Allowable	psi	Bending OK	Bending OK	
E A. Hand	:	59.9	67.3	
fv : Actual Fv : Allowable	psi psi	118.8	97.5 197.5	
rv : Allowable	psi	Shear OK	Shear OK	
Reactions				
O Lab End DI		1,127.00	1.576.00	
@ Left End DL LL	lbs lbs	1,008.00	1,408.00	
Max. DL+LL	ibs	2,135.00	2,984.00	
		ì	•	
@ Right End DL	lbs	1,127.00 1,008.00	1,576.00 1,408.00	
LL Max, DL+LL	lbs lbs	2,135.00	2.984.00	
	1170			With the second
Deflections		Ratio OK	Deflection OK	
Center DL Defl	in	-0.025	-0.280	
L/Defl Ratio		3,409.2	686.2	
Center LL Defl	in	-0.022	-0.250	
L/Defl Ratio		3,811.7	768.1	
Center Total Defl	in	-0.047	-0.530	
Location	ft		8.000	
L/Defl Ratio		1,799.6	<b>362</b> .4	



### Truss 1

VisualAnalysis 4.00 Report

Company: Paul Zacher - Structural Engineers Engineer: Paul Zacher

File: C:\Documents and Settings\Paul Zacher\Desktop\Matt04\_168\Truss 1.vap

### **Nodes**

Node	x ft	Y ft	Fix	DX	Fix	DY	Fix	RZ
N1	0.00	0.00	Yes		Yes		No	
N2	21.00	0.00	$N \circ$		"		Yes	
N3	10.50	3.50	"		No		No	
N4	10.50	0.00	"		"		"	
N5	5.25	1.75	"		"		"	
N6	15.75	1.75	**		"		,,	

### **Member Elements**

Member	Section	Material	Length ft
M1-2	SS2x4	Wood	10.50
M1-3	"	"	10.50
M2-2	"	"	5.53
M2-3	**	"	5.53
M3-2	"	"	5.53
м3-3	"	"	5_53
м4	"	"	5.53
M5	"	"	3.50
M6	"	"	5.53

# **Section Properties**

Category Secti	ion Ax	Iz	Sz (+y)	8z (-y)
	in^2	in^4	in^3	in^3
Wood Sha SS2x4	5.25	5.36	3.06	3.06

# **Material Properties**

Material	Strength psi	Elasticity psi		Density 1b/ft^3
Wood	-NA-	1700000.00	0.36	40.47

### **Load Combination Summary**

Equation Case: UBC97 12.8a Combination: 1D+1Lr

Contributing Cases & Source

Dead Load (Dead loads)

Roof Live Load (Roof Live loads)

### **Nodal Reactions**

Node	Load Case	FX	FY	MZ
		<i>1b</i>	<i>1.</i> b	1b-ft
			7	

N1	UBC97	12.8a	0.00	695.10	-NA-
N2	"		-NA-	695.10	0.00

# **Member Results**

M1-2	1618.75 1618.75	-54.56	1b-ft	in	in
"		-54 56			
	1618 75		-98.79	0.02	-0.14
<i>11</i>		-24.46	39.45	0.02	-0.19
	1618.75	5.64	72.38	0.01	-0.17
"	1618.75	35.74	0.00	0.00	0.00
M1-3	1618.75	-35.74	0.00	0.05	0.00
"	1618.75	-5.64	72.38	0.04	-0.17
"	1618.75	24.46	39.45	0.03	-0.19
"	1618.75	54.56	-98.79	0.02	-0.14
M2-2	-1744.1	113.63	0.00	0 - 00	0.00
"	-1712.3	18.00	121.34	-0.00	-0.10
"	-1680.4	-77.62	66.35	-0.01	-0.13
"	-1648.5	-173.25	-164.97	-0.01	-0.13
M2-3	-1186.5	173.25	-164.97	-0.01	-0.13
"	-1154.6	77.62	66.35	-0.02	-0.18
"	-1122.8	-18.00	121.34	-0.02	-0.19
"	-1090.9	-113.63	0.00	-0.02	-0.14
M3-2	-1186.5	-173.25	-164.97	0.06	-0.12
"	-1154.6	-77.62	66.35	0.06	-0.16
"	-1122.8	18.00	121.34	0.06	-0.18
u	-1090.9	113.63	0.00	0.06	-0.12
M3-3	-1744.1	-113.63	0.00	0.04	0.01
"	-1712.3	-18.00	121.34	0.05	-0.09
11	-1680.4	77.62	66.35	0.05	-0.12
,,	-1648.5	173.25	-164.97	0.06	-0.12
M4	-577.51	0.00	0.00	0.07	-0.12
"	-577.51	0.00	0.00	0.07	-0.12
"	-577.51	0.00	0.00	0.07	-0.12
"	-577.51	0.00	0.00	0.07	-0.11
M5	474.37	0.00	0.00	-0.14	-0.02
M3	474.37	0.00	0.00	-0.14	-0.02
"	474.37	0.00	0.00	-0.14	-0.02
"	474.37	0.00	0.00	-0.14	-0.02
м6	-577.51	0.00	0.00	-0.03	-0.13
MO //	-577.51	0.00	0.00	-0.02	-0.14
"	-577.51 -577.51	0.00	0.00	-0.02	-0.13
,,	-577.51 -577.51	0.00	0.00	-0.02	-0.13

### BENDING & COMP: TRUSS 1 - MEMBER 2-2

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

**Grading:** 

2x or 4x Doug-fir larch: No. 2

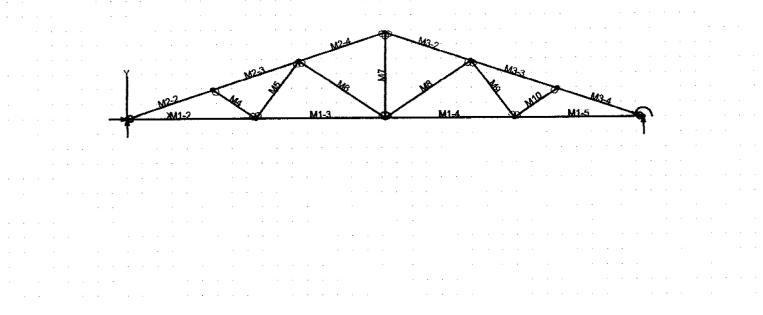
Assumptions:

Solid sheathing on top chord of truss. Therefore,

continuous lateral support is provided along compression face

Maximum center-center spacing = 24"

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Width, b	1.5 inches
Depth, d	3.5 inches
Length	5.53 feet
Max Axial Comp, C	1648 lbs
Max Reaction, R	173 lbs
Max Moment, M	164 ft-lbs
Max LL Deflection	0.07 inches
Max TL Deflection	0.13 inches
LL Defl Criteria = L/	240
TL Defl Criteria = L/	180
Duration factor, Cd	1.25
Repetitive Factor, Cr	1.15
Size Factor, Cf bending	1.5 1.5 for 2x4, 1.3 for 2x6
Size Factor, Cf comp	1.15 1.15 for 2x4, 1.1 for 2x6
Buckling Factor, CT =	1.15
fc =	314 psi
Fce=	1635 psi
Fc*=	2084 psi
F'c=	1255 psi
fb=	643 psi
F'b=Fb*=	2156 psi
Shear D/C ratio	0.42 < 1.0, Member OK
Interaction equation:	
(fc/F'c)^2 +	
fb/(F'b(1-fc/Fce)) =	0.43 < 1.0, Member OK
Live Load defl ratio	0.25 < 1.0, Member OK
Total Load defl ratio	0.35 < 1.0, Member OK



### Truss 2

VisualAnalysis 4.00 Report

Company: Paul Zacher - Structural Engineers Engineer: Paul Zacher

File: C:\Documents and Settings\Paul Zacher\Desktop\Matt04\_168\Truss 2.vap

### **Nodes**

Node	X ft	Y ft	Fix	DX Fix I	OY Fix RZ
N1	0.00	0.00	Yes	Yes	No
N2	34.50	0.00	Nο	"	Yes
м3	17.25	5.75	"	No	No
N4	8.63	0.00	"	"	"
N5	17.25	0.00	"	"	"
N6	25.88	0.00	"	"	"
N7	5.75	1.92	"	"	**
N8	11.50	3.83	"	"	"
N9	23.00	3.83	"	"	"
N10	28.75	1.92	"	"	"

## **Member Elements**

Member	Section	n Material	Length ft
M1-2	SS2x4	Wood	8.63
M1-3	"	"	8.63
M1-4	"	"	8.63
M1-5	"	"	8.63
M2-2	"	"	6.06
M2-3	"	"	6.06
M2-4	"	"	6.06
M3-2	"	"	6.06
M3-3	"	"	6.06
M3-4	"	er	6.06
м4	"	"	3.46
M5	"	"	4.79
M6	"	"	6.91
м7	"	"	5.75
M8	"	"	6.91
M9	"	"	4.79
M10	"	"	3.46

# **Section Properties**

Category	Section	Ax in^2	Iz in^4	Sz (+y) in^3	Sz (-y) in^3
Wood Sha	SS2x4	5.25	5.36	3.06	3.06

# **Material Properties**

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Material	Strength psi	Elasticity psi		Density 1b/ft^3
Wood	-NA-	1700000.00	0.36	40.47

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# Load Combination Summary Equation Case: UBC97 12.8a

Combination: 1D+1Lr

Contributing Cases & Source

Dead Load (Dead loads)

Roof Live Load (Roof Live loads)

### **Nodal Reactions**

Node	Load Case	FX 1b	FY <i>lb</i>	MZ lb-ft
N1 N2	UBC97 12.8a		<b>1141.95</b> 1141.95	-NA- 0.00

### **Member Results**

Member	Fx	Vy <i>1b</i>	Mz lb-ft	Dx in	Dy i <i>n</i>
	1b	ம	TD-LC		
<b>M</b> 1-2	2904.56	-40.97	-33.45	0.03	-0.35
"	2904.56	-16.24	48.76	0.02	-0.30
"	2904.56	8.48	59.91	0.01	-0.19
"	2904.56	33.21	0.00	0.00	0.00
11-3	2324.19	-39.61	-55.17	0.06	-0.38
"	2324.19	-14.88	23.13	0.05	-0.40
11	2324.19	9.84	30.37	0.04	-0-39
**	2324.19	34.57	-33.45	0.03	-0.35
11-4	2324.19	-34.57	-33.45	0.09	-0.35
"	2324.19	-9.84	30.37	0.08	-0.39
"	2324.19	14.88	23.13	0.07	-0.40
"	2324.19	39.61	-55.17	0.06	-0.38
11-5	2904.56	-33.21	0.00	0.12	0.00
"	2904.56	-8.48	59.91	0.11	-0.19
"	2904.56	16.24	48.76	0.10	-0.30
#	2904.56	40.97	-33.45	0.09	-0.35
12-2	-3106.1	133.34	0.00	0.00	0.00
"	-3071.2	28.61	163.51	-0.01	-0.20
"	-3036.3	-76.13	115.50	-0.02	-0.29
"	-3001.3	-180.86	-144.02	-0.02	-0.30
12-3	-2743.7	150.37	-144.02	-0.02	-0.30
"	-2708.8	45.63	53.89	-0.03	-0.35
"	-2673.9	-59.10	40.28	-0.04	-0.37
"	-2639.0	-163.84	-184.84	-0.05	-0.38
12-4	-1878.2	187.60	-184.84	-0.05	-0.38
"	-1843.3	82.86	88.29	-0.05	-0.45
"	-1808.4	-21.87	149.90	-0.06	-0.46
"	-1773 - 4	-126.61	0.00	-0.06	-0.38
<b>4</b> 3-2	-1878.2	-187.60	-184.84	0.16	-0.34
"	-1843.3	-82.86	88.29	0.17	-0.41
**	-1808.4	21.87	149.90	0.17	-0.43
″	-1773.4	126.61	0.00	0.18	-0.34
13-3	-2743.7	-150.37	-144.02	0.14	-0.26
"	-2708.8	-45.63	53.89	0.15	-0.31
"	-2673.9	59.10	40.28	0.15	-0.34
"	-2639.0	163.84	-184.84	0.16	-0.34
13-4	-3106.1	-133.34	0.00	0.12	0.04
"	-3071.2	-28.61	163.51	0.12	-0.16
"	-3036.3	76.13	115.50	0.13	-0.25
"	-3001.3	180.86	-144.02	0.14	-0.26
M4	-419.62	0.00	0.00	0.22	-0.2
"	-419.62	۵ ـ ۵	0.00	0.22	-0.25

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Member	F* 1b	Vy 1b	Mz Lb-ft	Dx in	Dy in
11	-419.62	0.00	0.00	0.22	-0.23
"	-419.62	0.00	0.00	0.22	-0.20
м5	385.38	0.00	0.00	-0.26	-0.25
"	385.38	0.00	0.00	-0.26	-0.23
"	385.38	0.00	0.00	-0.25	-0.28
"	385.38	0.00	0.00	-0.25	-0.27
M6	-723.12	0.00	0.00	0.26	-0.29
"	-723.12	0.00	0.00	0.27	-0.28
"	-723.12	0.00	0.00	0.27	-0.27
"	-723.12	0.00	0.00	0.27	-0.27
м7	881.44	0.00	0.00	-0.38	-0.06
"	881.44	0.00	0.00	-0.38	-0.06
"	881.44	0.00	0.00	-0.38	-0.06
"	881.44	0.00	0.00	-0.38	-0.06
M8	-723.12	0.00	0.00	-0.17	-0.34
"	-723.12	0.00	0.00	-0.17	-0.34
rr	-723.12	0.00	0.00	-0.16	-0.35
"	-723.12	0.00	0.00	-0.16	-0.35
м9	385.38	0.00	0.00	0.33	-0.19
"	385.38	0.00	0.00	0.33	-0.17
//	385.38	0.00	0.00	0.33	-0.15
"	385.38	0.00	0.00	0.33	-0.14
M10	-419.62	0.00	0.00	-0.12	-0.34
"	-419.62	0.00	0.00	-0.12	-0.31
"	-419.62	0.00	0.00	-0.12	-0.29
"	-419.62	0.00	0.00	-0.12	-0.27

### BENDING & COMP: TRUSS 2 - MEMBER 2-2

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

### Grading:

2x or 4x Doug-fir larch: No. 2

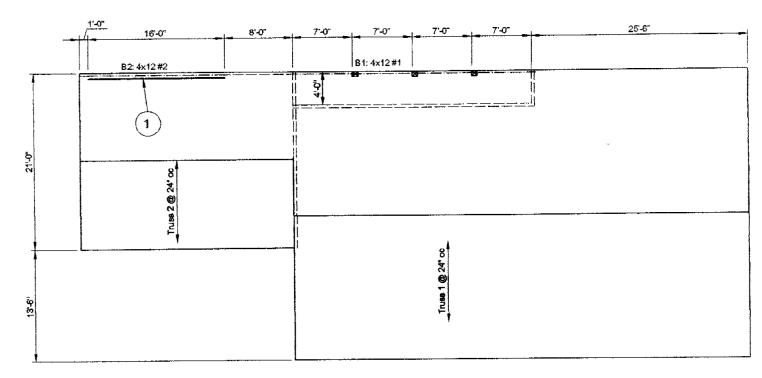
Assumptions:

Solid sheathing on top chord of truss. Therefore,

continuous lateral support is provided along compression face

Maximum center-center spacing = 24"

Width, b	1.5 inches
Depth, d	3.5 inches
Length	6.06 feet
Max Axial Comp, C	3001 lbs
Max Reaction, R	180 lbs
Max Moment, M	144 ft-lbs
Max LL Deflection	0.15 inches
Max TL Deflection	0.30 inches
LL Defl Criteria = L/	240
TL Defl Criteria = L/	180
Duration factor, Cd	1.25
Repetitive Factor, Cr	1.15
Size Factor, Cf bending	1.5 1.5 for 2x4, 1.3 for 2x6
Size Factor, Cf comp	1.15 1.15 for 2x4, 1.1 for 2x6
Buckling Factor, CT =	1.17
fc =	572 psi
Fce=	1378 psi
Fc*=	2084 psi
F'c=	1119 psi
fb=	564 psi
F'b=Fb*=	2156 psi
Shear D/C ratio	0.43 < 1.0, Member OK
Interaction equation:	
(fc/F'c)^2 +	
fb/(F'b(1-fc/Fce)) =	0.71 < 1.0, Member OK
Live Load defl ratio	0.50 < 1.0, Member OK
Total Load defl ratio	0.74 < 1.0, Member OK





### FRAMING NOTES:

1. Scab a 1 3/4" x 11 1/4" LVL to the existing 4x12 beam. See detail 2.

#### NOTES:

- A. This is a reroof project. The new roofing material shall be a Light Weight Concrete Tile. The tile shall weigh less than or equal to 7.3 psf..
- B. All structural wood members that were observed appear to be in sound condition and without structural defect.



