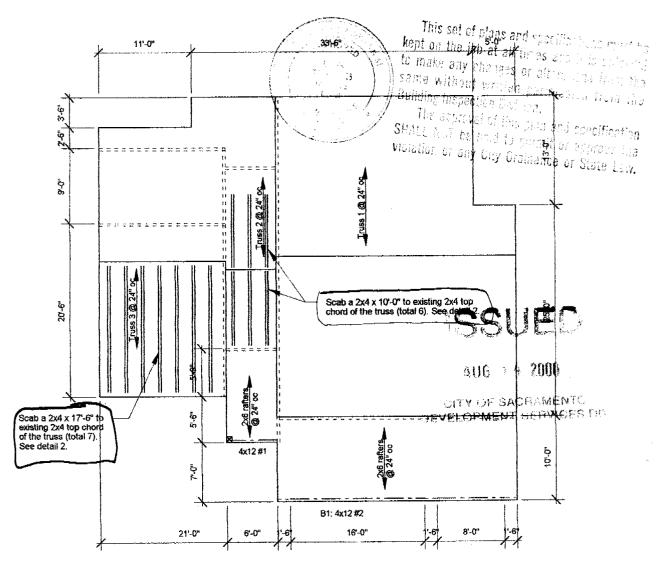
1231 I Street, Sacramento,	CA 95814	Insp Area: 2
· · · · · · · · · · · · · · · · · · ·	v. V	
Site Address: 301 BAY RIVE Parcel No: 031-0380-003	R WY SAC	Sub-Type: RES Housing (Y/N): N
CONTRACTOR  OF DICOUNTRY ROOFING	. <u>OWNER</u> KIMURA TOKUJI & JUDY	ARCHITECT
8296 ALPINE AVE	301 BAY RIVER WY	
S ACRANENTO CA 95826	SACRAMENTO CA 95831	
Nature of Work: 27 SQ T/O RES	HEET REROOF W PIONEER LT	WT TILE
CONSTRUCTION LENDING AGE of the work for which this permit is issued		erjury that there is a construction lending agency for the performance
Lender's Name	Lender'sA	ddress
LICENSED CONTRACTORS DEC		enalty of perjury that I am licensed under provisions of Chapter 9 nd my license is in full force and effect.
Lucense Class <u>4 - <b>3 1</b></u> Lucense Number_	622731 Date 8-14	Contractor Signature TM
		rjury that I am exempt from the contractors License Law for the ich requires a permit to construct, alter, improve, demolish, or repair
any structure, prior to its issuance, also req of the Contractors License Law (Chapter)	uires the applicant for such permit to file a 0 (commencing with Section 7000) of Div ged exemption. Any violation of Section 7	signed statement that he or she is licensed pursuant to the provisions ision 8 of the Business and Professions Code) or that he or she is 7031.5 by any applicant for a permit subjects the applicant to a civil
penalty of not more than five numbered dona	15 (\$500.00),	
for sale (Sec. 7044, Business and Professi thereon, and who does such work himself	onal Code: The Contractors License Lav or herself or through his/her own employed ment is sold within one year of completion	ssation, will do the work, and the structure is not intended or offered to does not apply to an owner of property who builds or improves so, provided that such improvements are not intended or offered for the owner-builder will have the burden of proving that he/she did
Code: The Contractors License Law does contractor(s) licensed pursuant to the Contr	not apply to an owner of property who bui actors License Law).	etors to construct the project (Sec. 7044, Business and Professions lds or improves thereon, and who contracts for such projects with a
Date	Owner Signature	
all measurements and locations shown on to or private agreement relating to permissible any improvement or the violation of any prince I certify that I have read this application a	he application or accompanying drawings a or prohibited locations for such improvem vate agreement relating to location of impr nd state that all information is correct. If	tes on the representation of the applicant, that the applicant verified and that the improvement to be constructed does not violate any law ents. This building permit does not authorize any illegal location of overents.  Agree to comply with all city and county ordinances and state laws ter upon the abovementioned property for inspection purposes.
		-1
Date 8 - 1 9 - 80	Applicant/Agent Signature	100
		nalty of perjury one of the following declarations: bensation as provided for by Section 3700 of the Labor Code, for the
performance of work for which the permit is	s issued.	·mO
I have and will maintain workers' cownich this permit is issued. My workers' co	ompensation insurance, as required by ser impensation insurance carrier and solve in	3700 of the Labor Code, for the performance of the work for mber are:
Carrier LEGION INSURANCE	Policy Number	260   260   We3-02985256   Exp Date 7/1/ <del>2000</del>
(This section need not be completed shall not employ any person in any manne subject to the workers' compensation provis	if the permit is for \$100 or less). I certify r so as to become subject to the white the ions of Section 3700 of a little white, 1 s	Exp Date 7/1/ <del>2000</del> 13. In the provision of the work for which this permit is issued, I suppressed in the provision laws of California and agree that if I should become hall forthwith comply with those provisions.
Date <b>%</b> -14-&)	Applicant Signature	$\mathcal{T}\mathcal{M}$
•		
CRIMINAL PENALTIES AND CIVIL FI	NES UP TO ONE HUNDRED THOUSA	EIS UNLAWFUL AND SHALL SUBJECT AN EMPLOYER TO AND DOLLARS (\$100,000) IN ADDITION TO THE COST OF ABOR CODE, INTEREST AND ATTORNEY'S FEE.

Permit No: 0009274

**CITY OF SACRAMENTO** 



See work regid, circled.

Matt P. 8/10/00



#### Notes:

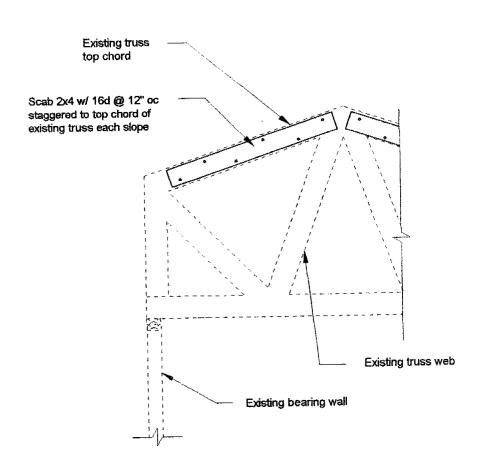
1. This is a reroof project. The new roofing material shall be a Light Weight Concrete Tile. The tile shall weigh less than or equal to 7.3 psf.

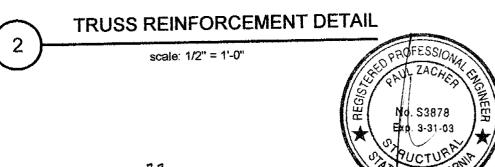
All structural wood members that were observed appear to be in sound condition and without structural defect.

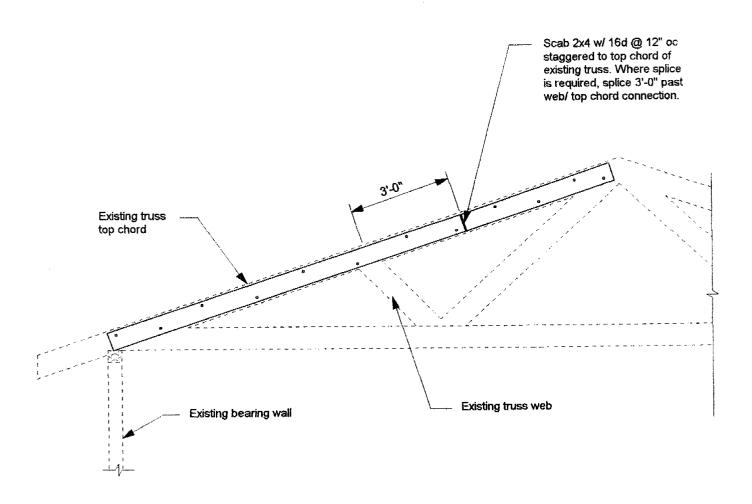
(1)

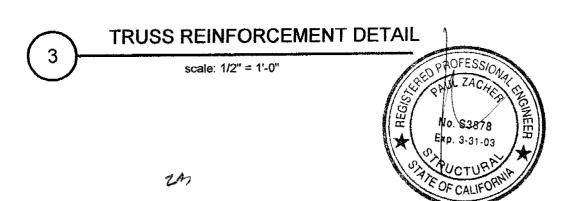
**ROOF PLAN - KIMURA** 

Not to Scale









Paul Zacher - Structural Engineers 4701 Lakeside Way Fair Oaks, CA 95628

xp. 3-31-03

August 3, 2000

**Old Country Roofing** 8296 Alpine Avenue Sacramento, CA 95826 TEL: (916) 453-8484 FAX: (916) 453-8487

Attn.: Mr. George Frank,

re: Job 2000\_194: KIMURA

Subject: Structural Investigation Report of the Roof for the Residence located at 301 Bay River Way, Sacramento, CA 95831.

As requested by Mr. George Frank, this is a report to determine what needs should be addressed to correct any structural deficiencies of the roof. Paul Zacher visited the site August 2, 2000. The investigation was made to determine the existing condition of the structure. All information, data and analysis contained within this report are based on the 1997 Uniform Building Code.

The following is based on visual observations with no subsurface investigation being made.

DESCRIPTION:

CQUU NGULBUMTTBUCETQU MEDLEGUM

Residence. Type of Facility:

Year Built:

Estimated 1980's vintage.

Occupancy:

Residential.

No. of Stories:

Two.

Dimensions:

Approximately 3000 square feet with a first story plate height of 8 feet.

#### CONSTRUCTION:

Roof:

The roof covering will consist of a Light Weight Concrete Tile over 1/2" solid sheathing. The living area is conventionally framed with 2x6 rafters spaced at 24" on center and with pre-engineered wood trusses spaced at 24" on center.

#### **CONCLUSIONS:**

Roof:

The living area has sufficient structural capacity for the applied live and dead loads. The garage lacks sufficient structural capacity for the applied live and dead loads.

1/20

Paul Zacher - Structural Engineers 4701 Lakeside Way Fair Oaks, CA 95628

#### **RECOMMENDATIONS:**

If any of the following recommendations do not correspond to actual field conditions, the engineer of record shall be notified for further investigation and evaluation before continuing work. Living Area:

1. Scab a 2x4 DF#2 rafter to the existing pre-engineered truss top chord with 16d's @ 12" on center. See details 1 and 2.

It shall be noted that small hairline cracking may occur at exterior stucco and interior gypboard finished walls that are load bearing or distributing roof strut loads. These cracks are a natural occurrence as the existing structure re-distributes the new roof weight. They are cosmetic in nature and are not an indication of a structural hazard or failure.

It shall be noted that some deflection of the rafters may be evident after installation of the tile. The existing roof framing has deflected but this may not be readily evident due to the uneven nature of the existing roofing material. Concrete tile is a very consistent and uniform product and when installed in an even plane, even small deflections can become apparent. This is only a cosmetic issue and not a structural concern.

The inspection consisted of visual observation only, made solely to determine the structural capacity of the existing roof. Analysis does not determine any effects on the overall structure under lateral forces or effects on the foundation unless specifically noted in the calculations and in this document. No warranties, expressed or implied, are made or intended in conjunction with this report. The inspection was made only to the portions that were accessible. The specific items noted were those that were observable and there may be defects that are not observable, or are hidden by architectural and structural materials.

If you have any questions on the above, do not hesitate to call.

Sincerely,

Paul Zacher, P.E., S.E.

file

## **DESIGN LOADING:**

Roof Pitch	6	in 12
Pitch Adjustment Factor	1.12	

## **LOCATION: ROOF**

MATERIAL	WEIGHT	· -
Light Weight Tile	7.30	psf
Roofing felt	0.30	psf
1/2" OSB/ plywood	1.50	psf
1x4 skip sht'g	1.09	psf
2x6 rafters @ 24" oc	<u>1.00</u>	psf
Load	11.2	psf
Roof Pitch Adjustment	1.32	psf
Total Load	12.5	psf

## LOCATION: TOP CHORD

<u>MATERIAL</u>	<b>WEIGHT</b>	
Light Weight Tile	7.30	psf
Roofing felt	0.30	psf
1/2" OSB/ plywood	1.50	psf
1x4 skip sht'g	1.09	psf
2x4 truss @ 24" oc	<u>1.28</u>	psf
Load	11.5	psf
Roof Pitch Adjustment	1.35	psf
Total Load	12.8	psf

# LOCATION: BOTTOM CHORD

MATERIAL	,	WEIGH	Γ
Batt/blown insul		0.50	psf
2x4 truss @ 24" oc		0.64	psf
1/2" Gypboard		2.50	psf
<i>.</i>	Load	3,6	psf

4701 Lakeside Way mer, S.E. Fair Oaks, CA 95628 TEL: (916) 961-3960 00-194 FAX: (916) 961-6552 Date: ال عدر موما 15/02 2×6+2 De 125 pur 20, 25 pvr Lp. 16.0. 2 - 52-65/80 181 4x 12 #2 0 p = 12,5 p.F = 50 + 05 p.F Les 160. - - 80 Page: 4

Lacher - Structural Engineers

701 Lakeside Way

Fair Oaks

TEL: (916) 961-3960 FAX: (916) 961-6552

Title: Dsgnr: Description :

Job#

Date: 1:39PM, 3 AUG 00

Scope:

Rev. 510304 User: KW-0602844, Vor 5.1.3, 22-Jun-1999, Win32 (c) 1983-99 ENERCALC

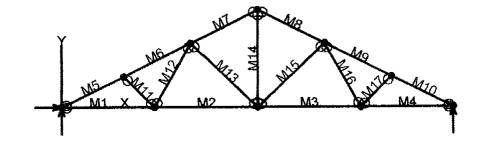
**Timber Beam & Joist** 

c:\enercalc\test ecw:Calculations

Description

RAFTERS AND BEAMS

Timber Member Information				Calculations are designed to 1997 NDS and 1997 UBC Requirements
		rafter	B1	
Timber Section		2x6	4x12	
Beam Width	in	1.500	3.500	
Beam Depth	in	5.500	11.250	
Le: Unbraced Length	Ħ	0.00	0.00	
Timber Grade	TY.	ouglas Fir - Larch,		
Fb - Basic Allow	psi	875.0	875.0	
Fy - Basic Allow	psi	95.0	95.0	
Elastic Modulus	ksi	1,600.0	1,600.0	
Load Duration Factor		1.250	1.250	
Member Type		Sawn	Sawn	
Repetitive Status		Repetitive	No	
Center Span Data	í			
Span	ft.	12.00	16.00	
·•	,			
Dead Load	#/ft	25.00	63.00	
Live Load	#/ft	32.00	80.00	
Results	Ratio ≃	0.9956	0.6182	
Mmax @ Center	in-k	12.31	54,91	
@X≖	ft	6.00	8.00	
fb : Actual	psi	1,628,0	743.8	
Fb : Allowable	psi	1,635,2	1,203,1	
1 10 1 7 111 00 1111	,	Bending OK	Bending OK	
fv : Actual	1	57.7	<b>38</b> .7	
Fv : Allowable	psi psi	118.8	118.8	
rv : Allowable	psi	Shear OK	Shear OK	
Reactions			·	
	التياسات			
@ Left End DL	ibs	150.00	504.00	
LL Many Division	lbs	192.00	640.00	
Max, DL+LL	lbs	342.00	1,144.00	
@ Right End DL	lbs	150.00	504.00	
ŁL.	ibs	192.00	640.00	
Max. DL+LL	lbs	342.00	1,144.00	
Deflections		Ratio OK	Deflection OK	
Center DL Defl	in	-0.351	-0.140	
L/Defl Ratio		410.8	1,373.3	
Center LL Defi	in	-0.449	-0.178	
L/Defl Ratio	111	320.9	1,081.5	
Center Total Defi	in	-0.799	-0.317	
Location	ft	6.000	8,000	
L/Defl Ratio		180.2	605.0	
L Den Made		1	555.5	



# sualAnalysis 3.50.c Report

08/03/00 12:20:00 Project: Truss 1

File: C:\Program Files\IES\VA35\truss 1.vap

Company: PK Associates Engineers

Engineer: Paul Zacher

Default Units: Feet, Pounds, Degrees, Fahrenheit, Seconds.

#### Nodes

Node	X ft	Y ft	Fix	DΧ	Fix	D¥	Fix	RZ
N1	0.00	0.00	Yes		Yes		No	
N2	9.00	0.00	No		No		"	
N3	19.00	0.00	"		"		**	
N4	29.00	0.00	"		**		"	
N5	38.00	0.00	"		Yes		"	
N6	6.00	3.00	"		No		#	
N7	32.00	3.00	"		"		"	
N8	12.50	6.25	"		"		"	
N9	25.50	6.25	"		"		"	
N10	19.00	9.50	"		"		"	

### Member Elements

Member	Section	Material	Length ft	
M1	SS2x4	Wood	9.00	
M2	F#	"	10.00	
мз	"	"	10.00	
M4	"	"	9.00	
M5	"	"	6.71	
M6	"	"	7.27	
M7	"	"	7.27	
M8	"	"	7.27	
M9	"	"	7.27	
M10	**	"	6.71	
M11	#	"	4.24	
M12	"	"	7.16	
M13	er e	"	9.02	
M14	rr	"	9.50	
M15	"	tr	9.02	
M16	"	"	7.16	
M17	"	rr .	4.24	

# Section Properties

Category	tegory Section		Iz in^4	Sy+ in^3	Sy- in^3
Wood Sha	SS2x4	5.25	5.36	3.06	3.06

# Material Properties

......

Material	Strength psi	Elasticity psi	Poisson	Density 1b/ft^3
Wood	-NA-	1700000.00	0.36	40.47

- The state of the

## Sad Combination Summary

Equation Case: Equation Case 1
Combination: +1D+1L+1Lr
Contributing Cases & Source
Service Case 1 (Dead loads)
Service Case 2 (Roof Live loads)

#### Member Uniform Loads

This item is empty. Check the selection state, or report properties.

### Nodal Reactions

Node	Load Case	FX lbs	FY 1bs	MZ lb-ft
N1 N5	Equation Case 1		1238.80 1238.80	-NA- -NA-

## Member Results

Member	Axial <i>1bs</i>	Vy <i>1bs</i>	Mz lb-ft	Dy in
 м1	2140.26	-40.01	-52.31	-0.2083
	2140.26	-17.21	33.3578	-0.1962
"	2140.26	5.5881	50.7934	-0.1366
"	2140.26	28.3881	0.0000	-0.0000
M2	1697.25	-39.24	-64.74	-0.2342
11	1697.25	-13.91	23.6361	-0.2638
"	1697.25	11.4231	27.7813	-0.2581
"	1697.25	36.7564	-52.31	-0.2083
МЗ	1697.25	-36.76	~52.31	-0.2083
",	1697.25	-11.42	27.7813	-0.2581
n	1697.25	13.9102	23.6361	-0.2638
"	1697.25	39.2436	-64.74	-0.2342
M4	2140.26	-28.39	0.0000	-0.0000
**	2140.26	-5.5881	50.7934	-0.1366
rr	2140.26	17.2119	33.3578	-0.1962
"	2140.26	40.0119	-52.31	-0.2083
M5	-2455.6			
"	-2404.1			
"	-2352.5			
"	-2301.0			
M6	-2186.39			
"	-2130.5	7 48.764	0 57.5416	
"	-2074.7			
"	-2018.9			
M7	-1493.3	1 201.3	3 - 246.33	
11	-1437.4			
**	-1381.6			
"	-1325.8			
м8	-1493.3			
"	-1437.4			
"	~1381.6			
"	-1325.8			
м9	-2186.3			
"	-2130.5			
"	-2074.7			
"	-2018.9			
M10	~2455.6			
"	-2404.1			

	-2352.58	80.604	1 99.751	5 -0.1763
	-2301.0	6 183.64	4 - 195.13	1 - 0.1403
M11	-362.64	-0.0000	-0.0000	-0.1290
"	-362.64	-0.0000	-0.0000	-0.1121
"	-362.64	-0.0000	-0.0000	-0.0953
"	-362.64	-0.0000	0.0000	-0.0785
M12	381.88	-0.0000	-0.0000	-0.1688
"	381.88	-0.0000	-0.0000	-0.1540
"	381.88	-0,0000	-0.0000	-0.1392
**	381.88	-0.0000	0.0000	-0.1244
M13	-626.54	0.0000	0.0000	-0.1351
"	-626.54	0.0000	0.0000	-0.1292
"	-626.54	0.0000	0.0000	-0.1233
#	-626.54	0.0000	0.0000	-0.1174
M14	947.01	-0.0000	-0.0000	-0.0487
ir .	947.01	-0.0000	-0.0000	-0.0487
"	947.01	-0.0000	-0.0000	-0.0487
"	947.01	-0.0000	0.0000	-0.0487
M15	-626.54	-0.0000	0.0000	-0.2026
**	-626.54	-0.0000	-0.0000	-0.1967
"	-626.54	-0.0000	-0.0000	-0.1908
"	-626.54	-0.0000	-0.0000	-0.1850
M16	381.88	-0.0000	0.0000	-0.0838
"	381.88	-0.0000	-0.0000	-0.0690
"	381.88	-0.0000	-0.0000	-0.0542
"	381.88	-0,0000	-0.0000	-0.0394
M17	-362.64	0.0000	0.0000	-0.1979
"	-362.64	0.0000	0.0000	-0.1810
"	-362.64	0.0000	0.0000	-0.1642
<i>"</i>	-362.64	0.0000	0.0000	-0.1474

### **BENDING & COMP: TRUSS 1 - MEMBER 5**

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

Grading:

2x or 4x Doug-fir larch: No. 2

Assumptions:

Solid sheathing on top chord of truss. Therefore,

continuous lateral support is provided along compression face

Maximum center-center spacing = 24"

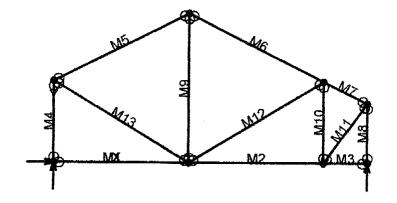
Width, b	1.5 inches
Depth, d	3.5 inches
Length	6.71 feet
Max Axial Comp, C	2301 lbs
Max Reaction, R	183 lbs
Max Moment, M	195 ft-lbs
Max LL Deflection	0.08 inches
Max TL Deflection	0.18 inches
LL Defl Criteria = L/	240
TL Defl Criteria = L/	180
Duration factor, Cd	1.25
Repetitive Factor, Cr	1.15
Size Factor, Cf bending	1.5 1.5 for 2x4, 1.3 for 2x6
Size Factor, Cf comp	1.15 1.15 for 2x4, 1.1 for 2x6
Buckling Factor, CT =	1.20
fc =	438 psi
Fce=	1085 psi
Fc*=	1869 psi
F'c=	911 <b>ps</b> i
fb=	764 psi
F'b=Fb*=	1887 psi
Shear D/C ratio	0.44 < 1.0, Member OK
Interaction equation:	
40 00 1 A 4 A 4	

 $(fc/F'c)^2 +$ 

 fb/ (F'b(1-fc/Fce)) =
 0.91 < 1.0, Member OK</td>

 Live Load defl ratio
 0.24 < 1.0, Member OK</td>

 Total Load defl ratio
 0.40 < 1.0, Member OK</td>



# dalAnalysis 3.50.c Report

s/03/00 12:51:49 Project: Truss 2

File: C:\Program Files\TES\VA35\truss 2.vap

Company: PK Associates Engineers

Engineer: Paul Zacher

Default Units: Feet, Pounds, Degrees, 'Fahrenheit, Seconds.

#### Nodes

Node	X ft	Y. £t	Fix	DX Fix	DY Fix RZ
N1	0.00	0.00	Yes	Yes	No
N2	9.25	0.00	No	No	"
N3	18.50	0.00	"	"	**
N4	21.50	0.00	"	Yes	"
N5	0.00	5.63	"	No	"
ие	9.25	10.25	"	"	"
N7	18.50	5.63	"	"	"
N8	21.50	4.13	"	"	″

### Member Elements

Member	Section	Material	Length ft
M1	SS2x4	Wood	9.25
M2	"	"	9.25
мз	"	"	3.00
M4	"	u	5.63
M5	"	rr	10.34
M6	"	"	10.34
M7	"	"	3.35
M8	"	"	4.13
м9	"	"	10.25
M10	"	**	5.63
M11	"	"	5.10
M12	н	"	10.83
M13	"	"	10.83

# Section Properties

Category	Section	Ax in^2	Iz in^4	Sy+ in^3	Sy- in^3
Wood Sha	ss2x4	5.25	5.36	3.06	3.06

# Material Properties

Material	Strength psi	Elasticity psi		Density 1b/ft^3
Wood	-NA-	1700000.00	0.36	40.47

# Load Combination Summary

Equation Case: Equation Case 1
Combination: +1D+1L+1Lr
Contributing Cases & Source

### Member Uniform Loads

This item is empty. Check the selection state, or report properties.

## Nodal Reactions

Node	Load Case	FX 1bs	FY <i>1bs</i>	MZ lb-ft
N1 N4	Equation Case 1	-0.00 -NA-	<b>700.90</b> 700.90	NA

## Member Results

Member	Azial 1bs	Vy 1bs	Mz <i>lb-ft</i>	Dy in
M1	0.0000	-42.81	-70.87	-0.0188
"	0.0000	-19.38	24.8227	-0.0608
"	0.0000	4.0546	48.4474	-0.0687
**	0.0000	27.4879	0.0000	-0.0000
M2	412.16	-30.98	-32.32	-0.0123
"	412.16	-7.5488	26.8999	-0.0446
"	412.16	15.8846	14.0489	-0.0391
"	412.16	39.3179	-70.87	-0.0188
M3	0.0000	-0.6263	0.0000	-0.0000
	0.0000	6.9737	-3.1927	-0.0027
"	0.0000	14.5737	-13.97	-0.0061
	0.0000	22.1737	-32.32	-0.0123
M4	-673.41	0.0000	0.0000	-0.0010
" "	-673.41	0.0000	0.0000	-0.0007
"	-673.41	0.0000	0.0000	-0.0003
	-673.41	0.0000	0.0000	-0.0000
м5	-529.80	238.28	0.0000	-0.0050
"	-450.37	79.4251	546.23	-1.1382
"	-370.95	-79.43	546.23	-1.1430
"	-291.52	-238.28	0.0000	-0.0192
M6	-552.85	-284.38	-476.80	-0.0156
"	-473.42	-125.53	228.37	-0.5494
"	-394.00	33.3212	387.30	-0.6683
"	-314.57	192.17	0.0000	-0.0172
M7	-428.38	64.8754	0.0000	-0.0027
"	-402.62	116.39	-101.48	0.0307
"	-376.86	167.91	-260.41	0.0388
"	-351.10	219.43	-476.80	-0.0156
M8	-700.27	0.0000	0,0000	0.0017
"	-700.27	0.0000	0.0000	0.0029
"	-700.27	0.0000	0.0000	0.0040
"	-700.27	0.0000	0.0000	0.0051
<b>49</b>	-113.95	-0.0000	-0.0000	0.0000
"	-113.95	-0.0000	-0.0000	0.0007
"	-113.95	-0.0000	-0.0000	0.0015
"	-113.95	-0.0000	0.0000	0.0022
<b>41</b> 0	-513.57	-0.0000	0.0000	-0.0025
"	-513.57	-0.0000	-0.0000	0.0001
**	-513.57	-0.0000	-0.0000	0.0026
"	-513.57	-0.0000	-0.0000	0.0051
M11	700.75	0.0000	0.0000	0.0037
"	700.75	0.0000	0.0000	0.0062
"	700.75	0.0000	0.0000	0.0088
"	700.75	0.0000	0.0000	0.0114

	-52.50	0.0000	0.0000	0.0125
	-52.50	0.0000	0.0000	0.0137
	-52.50	0.0000	0.0000	0.0149
"	-52.50	0.0000	0.0000	0.0160
M13	429.89	-0.0000	-0.0000	0.0038
"	429.89	-0.0000	-0.0000	0.0079
"	429.89	-0.0000	-0.0000	0.0120
"	429.89	-0.0000	0.0000	0.0160

## BENDING & COMP: TRUSS 2 - MEMBER6

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

### Grading:

2x or 4x Doug-fir larch: No. 2

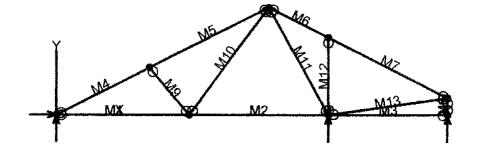
Assumptions:

Solid sheathing on top chord of truss. Therefore,

continuous lateral support is provided along compression face

Maximum center-center spacing = 24"

3 inches
3.5 inches
10.34 feet
552 lbs
284 lbs
476 ft-lbs
0.08 inches
0.18 inches
240
180
1.25
1.15
1.5 1.5 for 2x4, 1.3 for 2x6
1.15 1.15 for 2x4, 1.1 for 2x6
1.30
53 psi
497 psi
1869 psi
466 psi
933 <b>ps</b> i
1887 psi
0.34 < 1.0, Member OK
0.57 < 1.0, Member OK
0.15 < 1.0, Member OK
0.26 < 1.0, Member OK



# SualAnalysis 3.50.c Report

a8/03/00 13:14:05 Project: Truss 3

File: C:\Program Files\IES\VA35\truss 3.vap

Company: PK Associates Engineers

Engineer: Paul Zacher

Default Units: Feet, Pounds, Degrees, 'Fahrenheit, Seconds.

#### Nodes

Node	X ft	Y ft	Fix	DX Fix	DY Fiz	RZ
N1	0.00	0.00	Yes	Yes	No	
N2	10.00	0.00	No	No	"	
N3	20.50	0.00	"	Yes	"	
N4	29.50	0.00	"	"	"	
N5	7.00	3.50	"	No	"	
N6	29.50	1.25	"	"	er	
N7	16.00	8.00	**	"	"	
N8	20.50	5.75	"	"	"	

#### Member Elements

Member	Section	Material	Length ft
M1	SS2x4	Wood	10.00
M2	"	"	10.50
мз	"	"	9.00
M4	"	"	7.83
M5	"	"	10.06
M6	"	"	5.03
M7	"	#	10.06
M8	"	H	1.25
M9	"	"	4.61
M10	"	tt.	10.00
M11	"	"	9.18
M12	"	11	5.75
M13	"	"	9.09

# Section Properties

Category	Section	Ax in^2	Iz in^4	Sy+ in^3	sy- in^3
Wood Sha	SS2x4	5.25	5.36	3.06	3.06

# Material Properties

Material	Strength psi	Elasticity psi		Density 1b/ft^3
Wood	-NA-	1700000.00	0.36	40.47

# Load Combination Summary

Equation Case: Equation Case 1
Combination: +1D+1L+1Lr
Contributing Cases & Source

## Member Uniform Loads

This item is empty. Check the selection state, or report properties.

## Nodal Reactions

Node	Load Case	FX lbs	FY <i>1bs</i>	MZ 1b-ft
N1	Equation Case 1	0.00	572.38	-NA-
N3	ñ.	-NA-	1276.11	-NA-
N4	"	-NA-	74.91	-NA-

# Member Results

Member	Axial	Vу	Mz	Dy
	lbs	lbs	lb-ft	in
M1	815.70	-45.37	-73.70	-0.0460
"	815.70	-20.04	35.1018	-0.1073
**	815.70	5.2969	59.6676	-0.1091
"	815.70	30.6303	0.0000	-0.0000
M2	98.0796	-40.08	-75 - 62	-0.0000
"	98.0796	-13.48	17.8871	-0.0398
"	98.0796	13.1167	18.5286	-0.0556
"	98.0796	39.7167	-73.70	-0.0460
M3	0.0000	-25.80	-0.0000	-0.0000
"	0.0000	-2.9976	43.0218	-0.0495
"	0.0000	19.8024	17.8146	-0.0352
	0.0000	42.6024	-75.62	-0.0000
M4	-971.86	119.76	0.0000	-0.0000
"	-911.76	-0.4503	154.84	-0.1151
,,	-851.65	-120.66	-3.1332	-0.0640
	-791.55	-240.87 278.93	- <b>473.92</b> -473.92	-0.0491 -0.0491
M5	-661.59 -584.32	124.38	201.15	-0.4891
"	-584.34	-30.18	359.13	-0.5896
"	-307.04 -429.76	-184.74	0.0000	-0.0157
M6	180.14	-203.56	-440.92	-0.0025
"	218.77	-126.28	-164,67	0.0578
"	257.41	-49.00	-17.70	0.0251
"	296.05	28.2794	0.0000	-0.0227
<b>M</b> 7	187.91	-188.02	0.0000	0.0041
"	265.18	-33.46	370.13	-0.5922
"	342.46	121.10	223.16	-0,4905
"	419.74	275.65	-440.92	-0.0025
м8	-49.11	0.0000	0.0000	0.0092
rr .	-49.11	0.0000	0.0000	0.0103
**	-49.11	0.0000	0.0000	0.0113
"	-49.11	0.0000	0.0000	0.0124
м9	-535.80	0.0000	0.0000	-0.0216
"	-535.80	0.0000	0.0000	-0.0214
"	-535.80	0.0000	0.0000	-0.0211
. "	-535.80	0.0000	0.0000	-0.0209
M10	614.87	0.0000	0.0000	-0.0364
"	614.87	0.0000	0.0000	-0.0264
"	614.87	0.0000	0.0000	-0.0165
	614.87	0.0000	0.0000	-0.0066 -0.0174
M11	-714.38	0.0000	0.0000	-0.00174
"	-714.38	0.0000	0.0000	0.0014
••	-714.38	0.0000	0.0000	0.0014

سند معيده بديديد ( ١٠ معنيف يعنده سنده و ١٠٠٠ معنده بنديد بدر ١٠٠٠ معنده و المستعدد و ال

	-714.38	0.0000	0.0000	0.0108
1	-535.77	0.0000	0.0000	-0.0124
"	-535.77	0.0000	0.0000	-0.0091
"	-535.77	0.0000	0.0000	-0.0058
"	-535.77	0.0000	0.0000	-0.0026
M13	-254.57	-0.0000	0.0000	-0.0017
"	-254.57	-0.0000	-0.0000	-0.0016
"	-254.57	-0.0000	-0.0000	-0.0015
"	-254.57	-0.0000	-0.0000	-0.0014

### **BENDING & COMP: TRUSS 3 - MEMBER 4**

Design based on 1997 UBC 2321 Division V and ANSI/TPI 1-1995

Grading:

2x or 4x Doug-fir larch: No. 2

Assumptions:

Solid sheathing on top chord of truss. Therefore,

continuous lateral support is provided along compression face

Maximum center-center spacing = 24"

Width, b	3 inches
Depth, d	3.5 inches
Length	7,83 feet
Max Axial Comp, C	791 lbs
Max Reaction, R	240 lbs
Max Moment, M	473 ft-lbs
Max LL Deflection	0.02 inches
Max TL Deflection	0.04 inches
LL Defl Criteria = L/	240
TL Defl Criteria = L/	180
Duration factor, Cd	1.25
Repetitive Factor, Cr	1.15
Size Factor, Cf bending	1.5 1.5 for 2x4, 1.3 for 2x6
Size Factor, Cf comp	1.15 1.15 for 2x4, 1.1 for 2x6
Buckling Factor, CT =	1.23
fc =	75 psi
Fce=	818 psi
Fc*=	1869 psi
F'c=	726 psi
fb=	927 psi
F'b=Fb*=	1887 psi
Shear D/C ratio	0.29 < 1.0, Member OK
Interaction equation:	
(fc/F'c)^2 +	
fb/(F'b(1-fc/Fce)) =	0.55 < 1.0, Member OK
Live Load defl ratio	0.05 < 1.0, Member OK
Total Load defl ratio	0.08 < 1.0, Member OK